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# High-performance bismuth telluride thermoelectric thin films fabricated by using the two-step single-source thermal evaporation

Ping Fan <sup>a</sup>, Peng-cheng Zhang <sup>a</sup>, Guang-xing Liang <sup>a</sup>, Fu Li <sup>a</sup>, Yue-xing Chen <sup>a</sup>, Jing-ting Luo <sup>a</sup>, Xiang-hua Zhang <sup>b</sup>, Shuo Chen <sup>a</sup>, Zhuang-hao Zheng <sup>a,\*</sup>,

a. Shenzhen Key Laboratory of Advanced Thin Films and Applications, College of Physics and Optoelectronic Engineering, Shenzhen University, Shenzhen, 518060, China.

b. University Rennes, CNRS, ISCR (Institut des Sciences Chimiques de Rennes) – UMR 6226, F-35000 Rennes, France.

\* Corresponding Author, Email: zhengzh@szu.edu.cn

**Abstract** Bismuth telluride ( $\text{Bi}_2\text{Te}_3$ ) is an efficient thermoelectric material, and fabricating  $\text{Bi}_2\text{Te}_3$  thin films with good thermoelectric properties is a prerequisite to realizing the potential of these materials in microdevice application. Controllable content deposition and low-negative thermal treatment are the two main challenges in preparing high-performance thin films. In this study, stoichiometric  $\text{Bi}_2\text{Te}_3$  thin films were successfully fabricated via the two-step thermal vapor process with a single evaporation source. Then, the rapid thermal process, which could avoid component loss, was used to further improve the crystallinity and thermoelectric properties of thin films. The Seebeck coefficient of  $\text{Bi}_2\text{Te}_3$  thin films clearly increased after rapid heat treatment, leading to enhanced power factor and good flexibility. Such thin films exhibited low thermal conductivity due to their nano-sized grains, resulting in high ZT of flexible  $\text{Bi}_2\text{Te}_3$  thin films.

**Keywords:**  $\text{Bi}_2\text{Te}_3$  thin film; Thermal evaporation; Two-step process; Single source; Thermoelectric properties

## 1. Introduction

Given that thermoelectric (TE) materials can directly convert heat energy to electricity, they have great potential application in semiconductor cooling and generator fields [1]. The efficiency of TE materials is related to the dimensionless figure of merit, which is expressed as  $ZT = S\sigma T/(\kappa_L + \kappa_e)$ , where  $S$  is the Seebeck coefficient;  $\sigma$  is the electrical conductivity;  $T$  is the absolute temperature; and  $\kappa_L$  and  $\kappa_e$  are the lattice and electrical thermal conductivities, respectively [2]. Several applications have used minimal microwatts of power at high voltages in the operation of mobile electric devices and sensor network systems in the microelectronic industry [3-5]. A TE generator may be an ideal onboard power source in such cases. However, traditional techniques for manufacturing TE materials cannot meet the requirements, such as microsize, lightweight, flexible, and wearable, of these miniaturized devices. Thus, the preparation of TE materials as thin film onto a flexible substrate by using physical or chemical deposition is a promising technology to realize practical microsize and flexible TE materials [6].

Despite the  $ZT$  value of more than 2 in various novel TE materials, the classic bismuth telluride ( $\text{Bi}_2\text{Te}_3$ ) remains to be an excellent TE material due to its high TE performance at room temperature [7]. The majority of microsize or flexible devices are used commercially at low temperatures. Thus, many studies have investigated the preparation of high-performance  $\text{Bi}_2\text{Te}_3$  thin films [8-10]. Jin et al. fabricated  $\text{Bi}_2\text{Te}_3$  thin film with high  $ZT$  value and excellent flexibility for highly ordered (0001)-textured nanocrystals on high-quality SWCNT bundles via the sputtering

method [11]. The majority of studies have focused on preparing high-power factor  $\text{Bi}_2\text{Te}_3$  thin films through the development of thin film growth methods due to the difficulty in the precise measurement of thin film thermal conductivity [12-15].

Thermal evaporation is a promising thin film deposition technique that has also been used in the preparation of  $\text{Bi}_2\text{Te}_3$  thin films [16-18]. However, controlling the composition content of thin films with a single evaporation source is difficult because Bi and Te have distinctly different evaporation rates. Thus, the coevaporation method is commonly used to prepare  $\text{Bi}_2\text{Te}_3$  thin films from Bi and Te sources. Rogacheva et al. determined that the preferential growth direction of films prepared by coevaporation was related to the preparation conditions that have a significant effect on the TE properties of thin films [19]. However, the coevaporation method has difficulty in balancing the rate of the two sources and controlling the reaction between different vapor sources that easily leads to impurity phases. Additionally,  $\text{Bi}_2\text{Te}_3$  thin films prepared at room temperature exhibit poor crystallinity, and high-temperature heat treatment is needed to improve the crystallinity and TE properties [20-22]. However, some Te vacancy defects easily occur in Te-based materials because of its high saturated vapor pressure that will be reevaporated from the grain boundary during heat treatment [23-24]. Some organic materials, such as polyethylene terephthalate and polyimide, have been used as substrates to make the inorganic TE thin films flexible [25]. The majority of these organic materials cannot be used at high temperature for prolonged periods of time. Thus, the traditional annealing process could result in poor flexural mechanical and adhesion properties with the substrate.

In this study, we demonstrate a facile and efficient method for fabricating  $\text{Bi}_2\text{Te}_3$  thin films by using a single-source physical vapor deposition method. This method is different from the previous dual-source vapor evaporation because the composition of films can be easily controlled by using a two-step evaporation process. Furthermore, rapid thermal processing was used to optimize the TE properties of films to avoid element re-evaporation and flexible substrate damage. Hence, stoichiometric and highly uniform  $\text{Bi}_2\text{Te}_3$  thin films with good TE properties were successfully fabricated.

## **2. Experimental**

### **2.1 Material preparation**

$\text{Bi}_2\text{Te}_3$  powder was synthesized by using the mechanical alloying method. Stoichiometric mixtures of commercial powders Bi (4 N) and Te (4 N) were roughly mixed with a pestle and subjected to mechanical alloying in argon atmosphere. Milling was performed at 450 rpm for 6 hours in a planetary ball mill with a powder-to-ball mass ratio of 1:20. The results show that the prepared powder has a stoichiometric ratio and a single  $\text{Bi}_2\text{Te}_3$  phase (Fig. S1).

### **2.2 Film preparation**

The prepared  $\text{Bi}_2\text{Te}_3$  powder was used to fabricate  $\text{Bi}_2\text{Te}_3$  thin films by using the single-source thermal evaporation method. Polyimide (20 mm  $\times$  20 mm  $\times$  0.125 mm) was used as the substrate and ultrasonically and sequentially cleaned in acetone, alcohol, and deionized water.  $\text{Bi}_2\text{Te}_3$  powder (1 g) was placed into a crucible in a high-vacuum chamber with a basic pressure of  $1 \times 10^{-3}$  Pa. The substrate holder was

rotated at a rate of 5 rpm to ensure uniform evaporation. Evaporation current (EVC) was applied from 90 A to 120 A, and the deposition time remained constant for 10 min. Rapid heat treatment (RHT) was used to treat the thin films under vacuum. The target temperature was set to 500 K, and the heat rates were set to 2, 3, 4, and 5 K/s without heat retention.

### **2.3 Characterization**

The phase structures of  $\text{Bi}_2\text{Te}_3$  thin films were characterized by using X-ray diffraction (XRD; Ultima IV; Rigaku, Japan) in the conventional  $\theta$ - $2\theta$  mode at a scanning rate of  $1^\circ/\text{min}$ . The surface morphology and composition of thin films were determined via a scanning electron microscope (SEM, Zeiss Supra 55) with an energy dispersive X-ray microanalysis system and atomic force microscope (AFM, CSPM5500). The film thickness was measured with a Dektak<sup>3</sup> ST surface profile measurement system (Ultima4; Rigaku, Japan). The chemical states of samples were analyzed by using an X-ray photoelectron spectroscope (XPS, Escalab 250Xi) with a monochromatic Al  $K_\alpha$  X-ray source with energy of 1486.6 eV. The Seebeck coefficient and electrical conductivity were obtained by using a Seebeck coefficient–electrical conductivity measuring system (SBA458; Netzsch, Germany). Thermal conductivity  $\kappa$  was measured via the Linseis thin film laser flash system (TF-LFA, LINSEIS, Germany) via time-domain thermoreflectance method. A 200 nm-thick Au thin film layer was sputtered on top of the  $\text{Bi}_2\text{Te}_3$  thin film before the measurement as the transport layer. Carrier concentration and Hall mobility were measured by using the Van der Pauw Hall measurement (HL5500PC, Nanometrics).

### 3. Results and discussion

Thin films were generally prepared at a certain EVC by using the traditional thermal evaporation method [26]. The prepared  $\text{Bi}_2\text{Te}_3$  thin film displays enlarged component deviation with the powder due to the different evaporation rates of Bi and Te with a single evaporation source. Such phenomenon is consistent with our experimental results listed in Table S1. Moreover, the films are Te-rich when  $\text{EVC} \leq 100$  A and become Bi-rich after higher currents were used. Thus, the two-step thermal vapor process was used to balance the Bi and Te contents in the thin film. Fig. 1 presents the diagram. The Te-rich layer was first deposited onto the glass substrate at 40 nm with an EVC of 90 A. EVC was increased to 120 A to continue depositing at the Bi-rich layer with thickness of 200 nm. Then, the as-deposited thin films were further treated by using the RHT method. Fig. 2 illustrates the results of the EDS analysis of thin films, in which the as-deposited thin film composition is similar to the atomic ratio of 2:3 (Fig. 2a). Although the RHT condition varied, film composition remained nearly the same (Fig. 2b). The inserted elemental mapping (Sample H2) also shows that Bi and Te are homogeneously distributed without elemental segregation. These results indicate the successful fabrication of the stoichiometric and highly uniform  $\text{Bi}_2\text{Te}_3$  thin films in this study.

Table 1 shows the room-temperature electrical conductivity  $\sigma$ , Seebeck coefficient  $S$ , carrier concentration  $n$ , and mobility  $\mu$  of all the thin films. All samples possess negative  $S$  values, thereby indicating the n-type conduction feature, which was consistent with the corresponding bulk materials [27]. For pristine sample H1,  $\sigma >$

500.2 S cm<sup>-1</sup>, which is similar to the value of stoichiometric Bi<sub>2</sub>Te<sub>3</sub> thin films [28-30]. However, obtained  $S$  is extremely low at only  $-10.1 \mu\text{V K}^{-1}$ . The poor  $S$  value is attributed to the very high  $n$  value, which is approximately two orders of magnitude higher than the optimal range of the Bi<sub>2</sub>Te<sub>3</sub> material at  $\sim 10^{19} \text{ cm}^{-3}$  [31]. The absolute  $S$  value of films remarkably increase from  $\sim 10 \mu\text{V K}^{-1}$  to over  $\sim 100 \mu\text{V K}^{-1}$  due to the substantial decrease in  $n$  after heat treatment, and their values are all in the optimal range. By contrast, electrical conductivity is only slightly reduced because of the gradual increase in mobility. Hence, the power factor of films is remarkably enhanced by approximately 10 times compared with that of the as-deposited sample at various RHT conditions. Figs. 3a and 3b show the temperature dependence of  $\sigma$  and  $S$  of samples H2–H5 in the range of 303–483 K. The  $\sigma$  value of films increases with the increase in temperature that suggests its semiconductor behavior. The absolute  $S$  value increases to a peak at  $\sim 350$  K and downshifts at higher temperatures. Fig. 3c presents the calculated power factor  $S^2\sigma$  and displays an increasing trend with temperature. Consequently, the film H4 prepared by using the heat rate of 4 K/s has a higher power factor than the others, and the maximum power factor of  $0.53 \text{ mW m}^{-1} \text{ K}^{-2}$  is obtained at 478 K. The changes in relative resistance ( $\Delta R/R_0$ , where  $\Delta R$  is the difference between the resistance after bending, and  $R_0$  is the origin resistance before bending) of sample H4 were measured to assess the bending flexibility of the thin film with the bending radius about 5 mm (Fig. 3d). The results show that the resistance deviation before and after bending is very small at only  $\sim 0.5\%$  within 200 cycles and  $\sim 2\%$  after



1000 cycles. This result indicating good flexibility is comparable to the reported results [11, 13].

Analyses were performed to further investigate the underlying factors for the significant changes in the property of the TE thin film because of the minimal differences in film composition. Fig. 4 shows the crystalline structure determined by XRD in the range of  $10^{\circ}$ – $80^{\circ}$ . The as-deposited sample obtains the strongest peak at  $\sim 27.5^{\circ}$ , which belongs to the (015) plane of the  $\text{Bi}_2\text{Te}_3$  phase. However, many impurity peaks are observed. Given its very high carrier concentration, we deduce that nonregular component defects are formed due to insufficient kinetic energy. This phenomenon results in weak atom migration when thin films are prepared at room temperature despite its stoichiometric composition. By contrast, the films show typical rhombohedral  $\text{Bi}_2\text{Te}_3$  diffraction peaks after heat treatment, and no impurity peak is observed within the detection limit, thereby indicating the single-crystal structure of the films. Thus, the improved crystallinity of RHT films remarkably enhances the TE properties. In particular, the peak intensity of the (006) plane evidently increases after heat treatment but only increases slightly when the heat rate is lower than  $4 \text{ K s}^{-1}$ , and (1010) becomes the strongest plane at  $2 \text{ K s}^{-1}$ . In many cases,  $\text{Bi}_2\text{Te}_3$  thin films with (00 $l$ ) have better TE properties than the other films [12, 13]. Thus, the change in the preferred orientation would have caused the different TE properties of the thin films prepared at various RHT conditions. To illustrate the results better, the samples were measured with the AFM, and the images are shown in Fig. 5a, which displays the average surface size of grains. The surface size increases

rapidly when the heat rate decreases from  $5 \text{ K s}^{-1}$  to  $4 \text{ K s}^{-1}$ , and further decreasing the heat rate reduces the effect. The  $\text{Bi}_2\text{Te}_3$  structure consists of Te1–Bi–Te2–Bi–Te1 quintuple layers along the c-direction and are weakly coupled with each other via the van der Waals interactions [31]. This feature structure results in the lower formation energies of (00 $l$ ) plane than those of the others [32]. Therefore, the nuclei gradually merges via heat treatment and preferentially grow to the a(b) direction, thereby causing the increase in the grain surface size. However, a prolonged treatment time will also intensify the atom diffusion across the grain interface and promote nuclear growth along the other orientations.

Fig. 6 shows the high-resolution core-level spectral regions of Bi4f and Te3d for the as-deposited sample and the samples heated at the rates of 2 and 3 K/s. The binding energy of all peaks is corrected by using the C1s energy at 284.4 eV in addition to the charge compensation via the flood gun associated with the spectrometer. Two peaks at energies of  $\sim 157$  and  $\sim 162$  eV are observed for all samples in Fig. 6a. These values correspond to the binding energy of  $\text{Bi}4f_{7/2}$  and  $\text{Bi}4f_{5/2}$  of single-crystal  $\text{Bi}_2\text{Te}_3$  [33]. For Te (Fig. 6b), the peaks are obtained at  $\sim 572$  and  $\sim 583$  eV, which are also consistent with the data observed from  $\text{Bi}_2\text{Te}_3$  [33]. The XPS results further prove the successful preparation of intermetallic  $\text{Bi}_2\text{Te}_3$  compounds. Additionally, the binding energies of Bi4f and Te3d peaks of the as-deposited thin film are slightly larger than that of the single crystal and demonstrate a red shift after RHT. Thus, the XRD results show that certain impurity electron groups may have an effect on the chemical interaction of the Bi-Te bond in

the as-deposited thin film and lead to the higher binding energy of the as-deposited thin film compared with that of pure Bi<sub>2</sub>Te<sub>3</sub>. The decrease in impurity defects decreases the binding energy of the thin film and becomes closer to that of the single-crystal Bi<sub>2</sub>Te<sub>3</sub>.

Fig. 7a shows the total thermal conductivity  $\kappa_{\text{total}}$  of samples H3 and H4. Lattice thermal conductivity  $\kappa_{\text{lat}}$  was also calculated (Fig. 7b) by using the formula  $\kappa_{\text{total}} = \kappa_{\text{lat}} + \kappa_{\text{ele}}$ , where  $\kappa_{\text{ele}}$  is the contribution of electrons.  $\kappa_{\text{ele}}$  is estimated via the Wiedemann–Franz law  $\kappa_{\text{ele}} = L\sigma T$ , where the constant L, also known as the Lorenz number, depends on the degree of elasticity in carrier scattering. The temperature dependence of the Lorenz number is calculated, and the results are provided in Table S2 [34]. The films have very low thermal conductivity, which is only ~70% of bulk Bi<sub>2</sub>Te<sub>3</sub> [35-38] due to the low lattice thermal conductivity. The AFM images demonstrate that the films have a grain size of ~100 nm. The SEM results also confirm that the films have smooth surfaces and nano-sized particles (see in Fig. S2). Thus, low thermal conductivity is attributed to the nanostructure (Fig. 7c), in which phonons with short wavelengths are effectively scattered by the nano-sized grains, whereas those with long wavelengths are scattered by the grain boundaries with large sizes. Fig. 7d shows the temperature dependence of the ZT value. The estimated maximum ZT values of ~0.47 and ~0.51 are achieved from samples H3 and H4 at ~400 K, respectively. These findings are comparable to the best results of flexible Bi<sub>2</sub>Te<sub>3</sub> thin films.

#### **4. Conclusions**

Bi<sub>2</sub>Te<sub>3</sub> thin films were synthesized with flexible substrates by using the two-step

single-source evaporation method at various rapid heat treatment rates. Stoichiometric Bi<sub>2</sub>Te<sub>3</sub> thin films with uniform element distribution were obtained, and the heat rate was crucial in the increase in the Seebeck coefficient. As predicted, the power factor was enhanced by approximately 10 times after RHT. Moreover, the nano-sized grains of thin films resulted in ultralow thermal conductivity, leading to their high ZT values. These findings are comparable to the best value of flexible Bi<sub>2</sub>Te<sub>3</sub> thin films. The results demonstrated the efficiency of this innovative technique for the preparation of high-performance flexible thermoelectric thin films.

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Table 1 Thermoelectric properties of thin films at room temperature

Sample	Heating rate (Ks <sup>-1</sup> )	$\sigma$ (Scm <sup>-1</sup> )	S (- $\mu$ VK <sup>-1</sup> )	PF (mWm <sup>-1</sup> K <sup>-2</sup> )	$n$ (cm <sup>-3</sup> )	$\mu$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )
H1	As-deposited	500.2	-10.1	0.005	1.41 $\times$ 10 <sup>21</sup>	2.17
H2	2	257.1	-128.4	0.424	4.39 $\times$ 10 <sup>19</sup>	39.4
H3	3	262.9	-125.9	0.416	4.61 $\times$ 10 <sup>19</sup>	38.7
H4	4	280.9	-125.7	0.444	4.80 $\times$ 10 <sup>19</sup>	34.7
H5	5	305.2	-118.8	0.431	5.03 $\times$ 10 <sup>19</sup>	32.3

## Figure Captions

**Figure 1** Schematic of the preparation of thin films

**Figure 2** (a) EDS test results of the as-deposited thin film and (b) atomic composition of thin films (inset: elemental mapping of sample H2)

**Figure 3** Temperature dependence of thin films after heat treatment: (a) electrical conductivity, (b) Seebeck coefficient, and (c) power factor; (d) bending test of sample H4

**Figure 4** Powder X-ray diffraction of all thin films

**Figure 5** AFM images of thin films after heat treatment

**Figure 6** Binding energy obtained from the high-resolution core-level spectral regions of (a) Bi4f and Te3d of the as-deposited sample and the samples prepared at heat rates of 1 and 3 Ks<sup>-1</sup>.

**Figure 7** (a) Total thermal conductivity and (b) the calculated lattice thermal conductivity of samples H3 and H4 as a function of temperature, (c) various phonon scattering mechanisms via the nanostructure and grain boundary defect, and (d) temperature dependence of the ZT value.

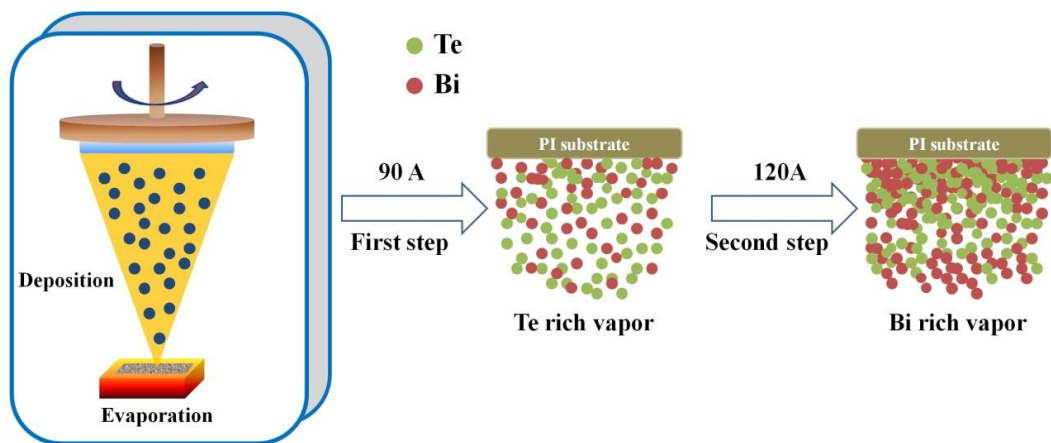


Figure 1

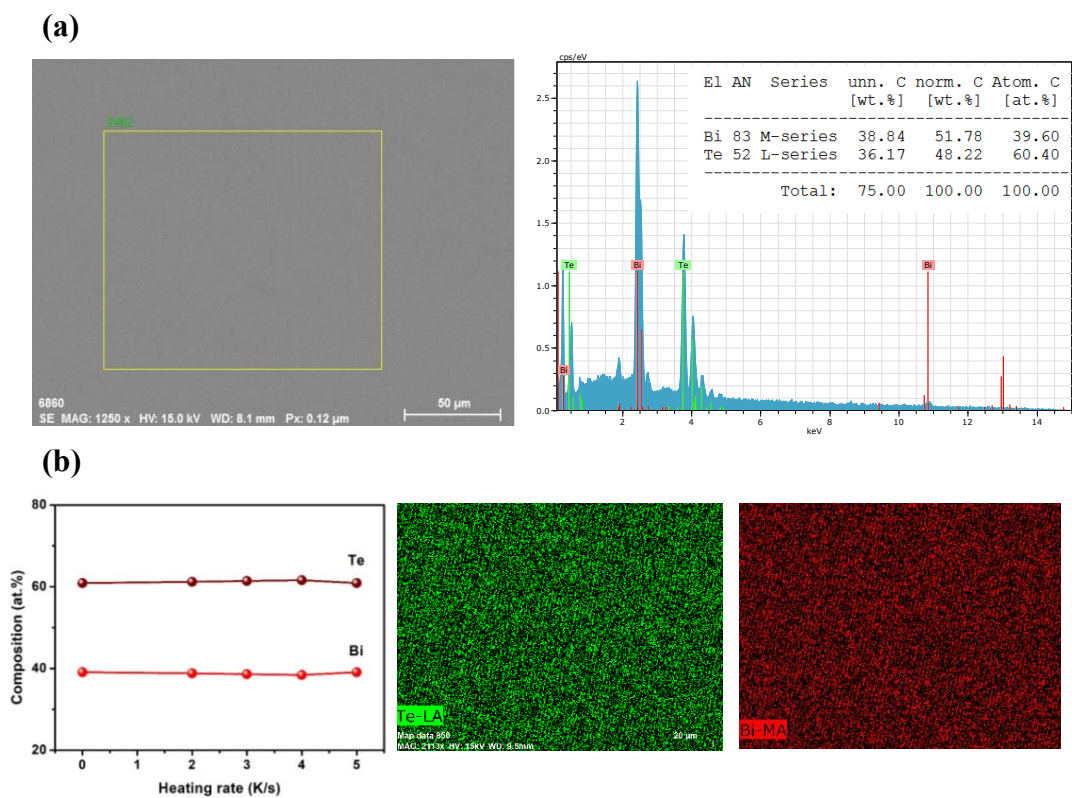


Figure 2

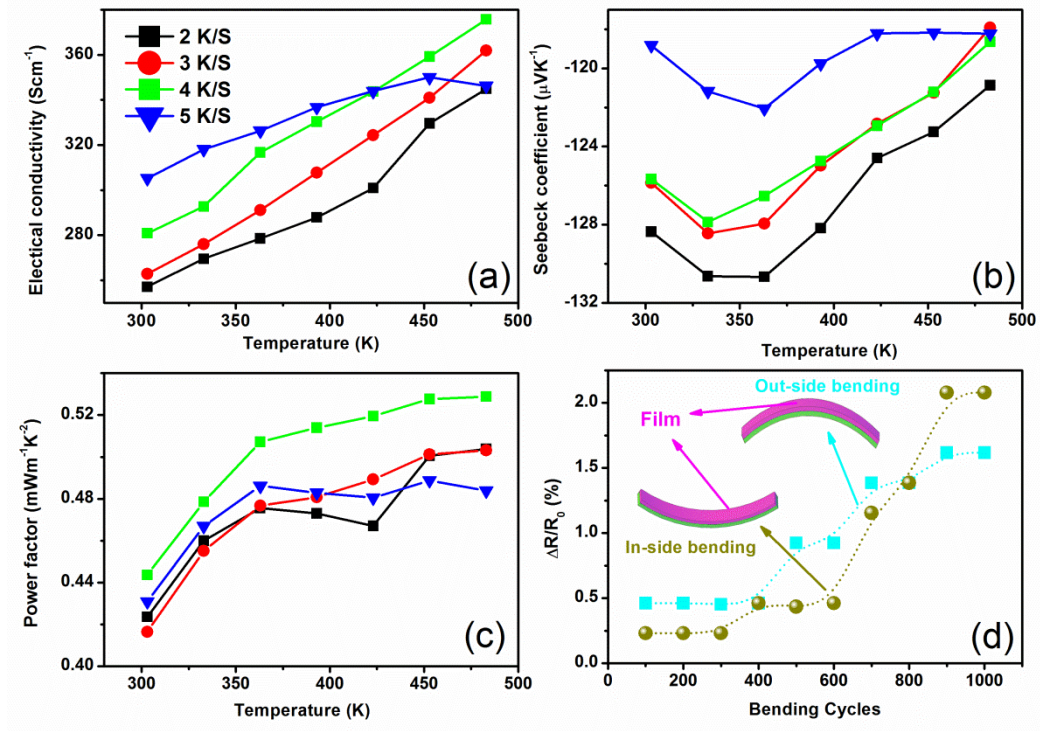


Figure 3

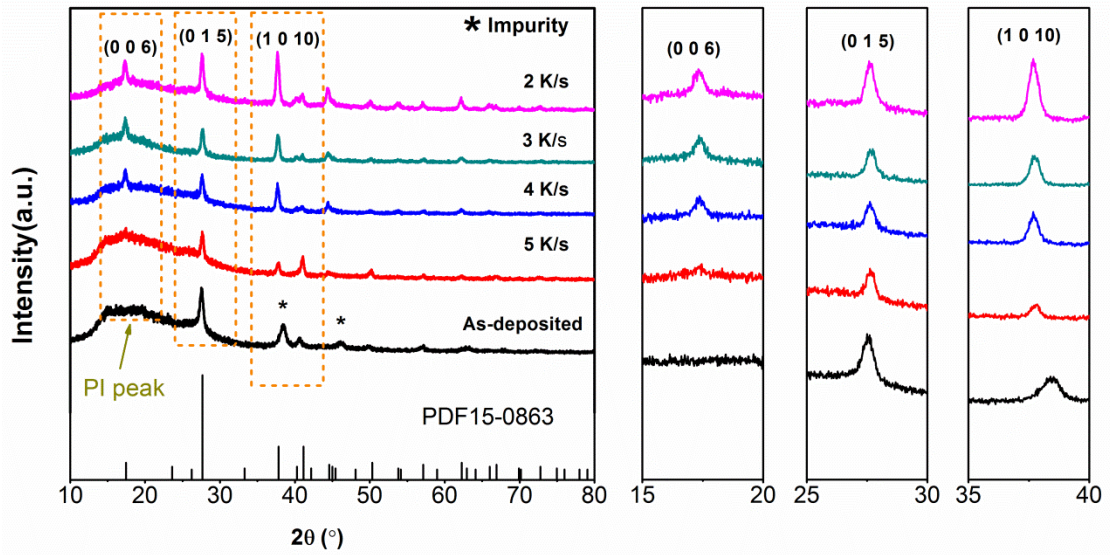
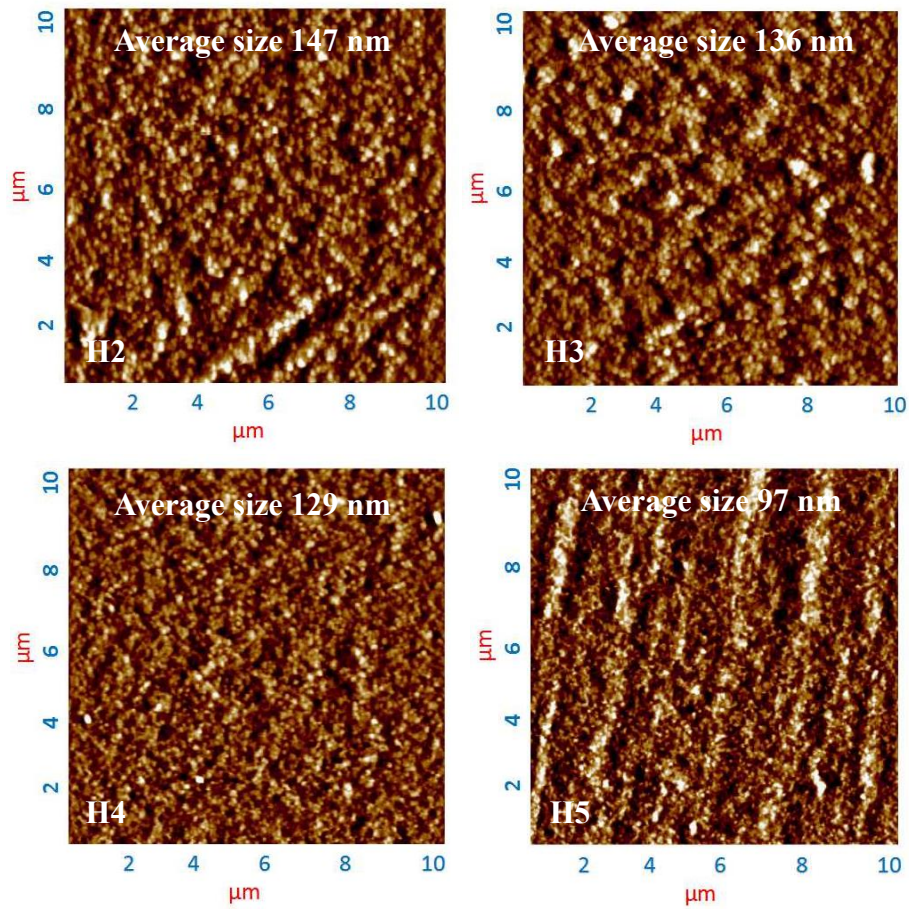
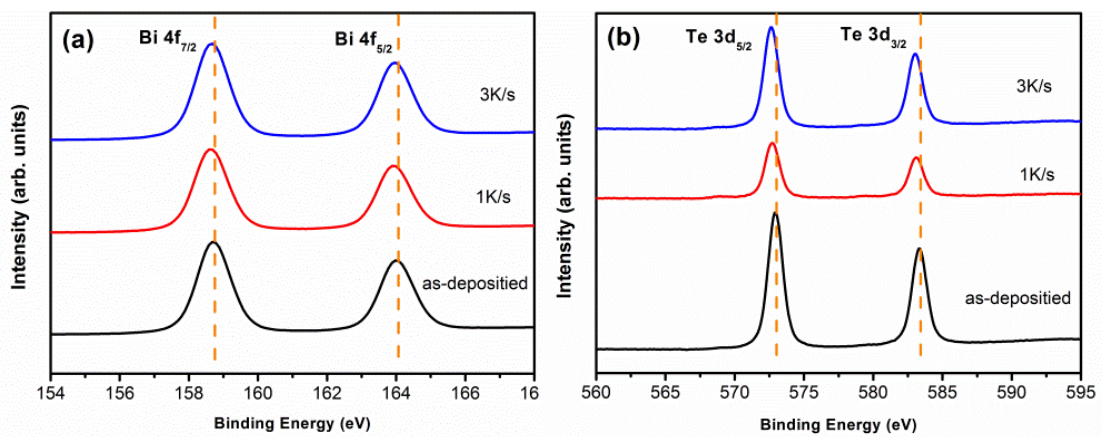


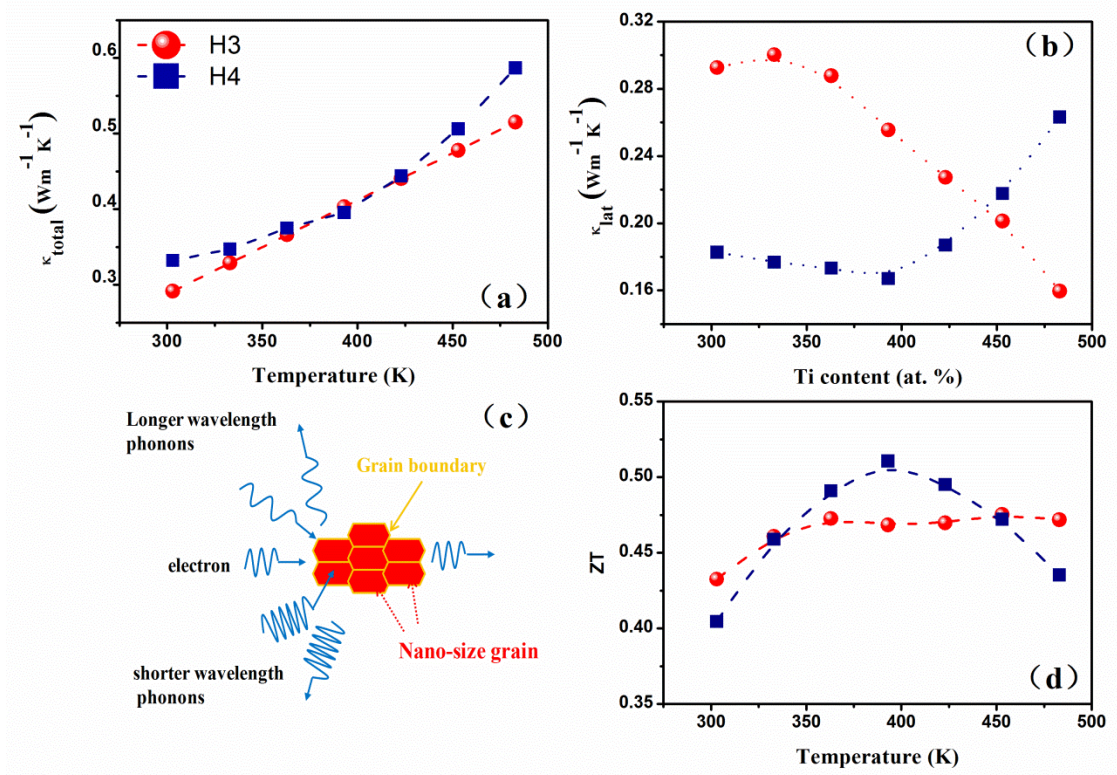
Figure 4



**Figure 5**



**Figure 6**



**Figure 7**