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Hygrothermal effects and moisture kinetics in a bio-based multi-layered wall: Experimental and numerical studies

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Abstract

A bio-based multi-layered reference wall has been developed within the framework of the European ISOBIO project. One of the key points of this project was to be able to perform proper simulations of the hygrothermal transfers occurring inside such walls. Previous published investigations, also performed in the framework of this project, have demonstrated that the classic assumption of instantaneous equilibrium between local relative humidity and water content according to the sorption isotherm is not relevant for bio-based porous materials, where, in practice, a rather slow kinetics of sorption occurs. The theoretical background developed in this previous study is used here to determine the kinetic constants of the bio-based construction materials and to perform 1D hygrothermal simulations. The kinetics constants are determined thanks to a 1D cylindrical tool based on the local kinetics approach, validated against several experiments of sorption. Then, heat and hygric transfers recorded on a demonstrator building (The HIVE, Wroughton, UK) are analyzed and are simulated using two modeling tools: TMC based on the Kunzel approach and TMCKIN based on the local kinetic approach. From the simulations, the local kinetics improves the small timescale *RH* dynamics. The comparison with measurements performed in the demonstrator confirms the relevance of the local kinetics approach.

Keywords

Bio-based building materials; Local kinetics; Sorption; Hygrothermal transfer; Mass transfer; Modeling

1 Introduction

The aim of the European ISOBIO project was to develop multi-layered wall solutions made of bio-based materials featuring very low carbon footprints and high insulating properties. The present study has been done in this framework. One of the key points of this project was to be able to perform proper simulations of the hygrothermal transfers occurring inside the ISOBIO reference wall.

Sorption of water in porous media involves interdependent phenomena such as vapor / liquid water mass transport by Fickian diffusion and equilibrium isotherms of sorption also called "water storage functions" associated with hysteretic phenomena. The diffusion coefficients can be determined in

steady state exchange by permeability measurements (*i.e.* "wet cup method" [1]). The equilibrium isotherms of sorption can be determined by gravimetric methods [2]. Actually, the equilibrium water contents evolve as a function of the relative humidities between the main adsorption and desorption equilibrium isotherms depending on the material's hygric history and this complex phenomenon can be described by hysteretic models [3, 4]. Note that heat and mass transfer phenomena have to be properly modeled and coupled, as highlighted in [5]: heat transfers in walls can have a significant effect on the hygric transfers and inversely. But despite the reliability of these models, it seems that inside some porous materials, and particularly in bio-based materials, simulations largely underestimate the time required for the water content to reach the equilibrium: this has been established for bio-based materials in [6, 7, 8] and by Reuge et al. [9], but also for more traditional material such as cement compounds or concretes [10, 11, 12]. These considerations take on their full meaning in the cases of hygrothermal transfers with permanent fluctuations such as in materials of building envelopes, in soils or in food materials.

Classic simulation tools predicting hygrothermal transfers in building materials are based on the assumption that for a given local relative humidity ϕ , the associated equilibrium local water content w is reached instantaneously. In our previous studies [9, 13], three hemp-lime concretes were studied and it was demonstrated that such an assumption led to serious inconsistencies. Thus, as reported in the aforementioned literature, our previous studies have established that a local kinetics of sorption exists (from water vapor to liquid water and inversely) which can be slow compared to the diffusive fluxes. Obviously, this invalidates the classic assumption.

The first part of this study deals with the classic hygric and thermal properties obtained from characterizations performed on samples of ISOBIO materials. From the knowledge of these classic properties, a simple steady-state sensitivity study is performed to determine the most sensitive layers in the ISOBIO reference wall in term of thermal transmittance and resistance to water vapor diffusion. Then, the theoretical background necessary to model the water sorption / kinetics of sorption is presented, relying on the study [9]. Thanks to this theoretical background, the kinetics constants of some of the studied ISOBIO materials are determined numerically and analytically by adjustments on sorption experiments. The last part of this study compares the results of the hygrothermal simulations based on the classic model with and without taking into account solar radiation and the local kinetics model to the measurements performed inside the ISOBIO reference wall at the HIVE demonstrator (Wroughton, UK) over a wide range of hygric and thermal operating conditions.

2 Classic hygrothermal properties of the ISOBIO materials

2.1 Reference ISOBIO wall

The reference ISOBIO wall is composed of: a BCBTM lime-hemp render (BCB), a CAVACTM Rigid insulation panel made of hemp shiv and an organic binder (CAV), a Biofib Trio flexible insulation panel from CAVACTM made of hemp flax and cotton (BIO), an OSB3 panel, a ProclimaTM INTELLO membrane (INT), a Lignicell CSBTM panel made of compressed straw (CSB) and a CLAYTECTM clay-hemp plaster (CLA). Note that this wall is supported by a timber frame which will not be considered in the simulations. The configuration and the thicknesses of the different layers are given in Figure 1.

Note that the local hygric variables given at the macroscopic scales will be written as lower case letters (*e.g.* the local water content w) while the hygric variables given at the sample scales will be written as upper case (*e.g.* the global water content W).

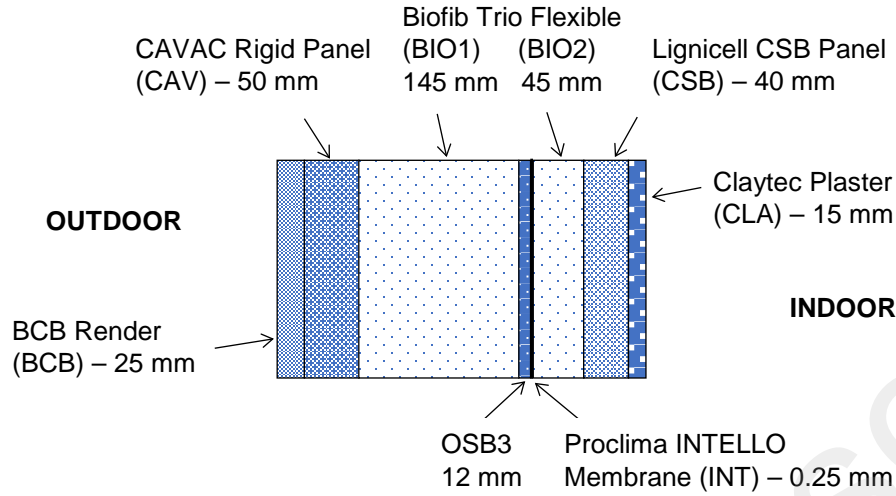


Figure 1: ISOBIO reference wall

2.2 Experimental characterizations

The experimental characterizations of the ISOBIO materials hygrothermal properties have been performed by Collet et al. [14]. Therefore, the experimental methods of measurement will not be described here but only the values of the properties necessary to perform the simulations.

Table 1 is a compilation of the following properties measured at a temperature of 23°C: the bulk densities at dry state ρ_0 , the porosities ϵ_0 , the vapor diffusion resistance factors at dry state μ_0 , the thermal conductivities at dry state λ_0 and the specific heat capacities at dry state C_{p_0} . Note that while most of these properties have been determined by Collet et al. [14], a few others have been determined by other ISOBIO partners (University of Bath for BCB permeability) or obtained from trustable technical sheets.

The adsorption behavior of representative samples of the ISOBIO materials (CAV, BIO, OSB3 and CSB) have been studied in [14]: they have measured their water content W (kg of water per m^3) temporal evolutions until quasi stabilization (or in other words, their global kinetics of adsorption) after several instantaneous increments of ambient relative humidity RH at a temperature T of 23°C. The final stabilized W are actually the equilibrium water contents W_{eq} at the corresponding RH , allowing to determine the adsorption isotherms of the materials. The moisture storage functions of the other ISOBIO materials come from technical sheets and/or F-IBP databases (BCB, INT and CLA). The data are shown in Figure 2.

2.3 Models of properties

From the collected data of W_{eq} as a function of RH , the Van Genuchten model VG [15] has been used to model the adsorption isotherms. Note that the VG model is claimed valid even at high RH (>90%). It is expressed as follow:

$$W_{eq}(RH) = W_{sat} \left[1 + (-h \ln(RH))^\eta \right]^{1/\eta-1} \quad (1)$$

where h and η are adjustment coefficients.

	ρ_0 $\pm 5\%$ (kg.m^{-3})	ε_0 $\pm 5\%$ (-)	μ_0 $\pm 10\%$ (-)	λ_0 $\pm 5\%$ ($\text{W.m}^{-1}.\text{K}^{-1}$)	Cp_0 $\pm 10\%$ ($\text{J.kg}^{-1}.\text{K}^{-1}$)
BCB	530	0.546	9	0.13	1006
CAV	190	0.874	11	0.07	2100
BIO	26.5	0.98	3.6	0.039	1800
OSB3	551	0.609	138	0.13	1600
INT	85	0.085	$1.364.10^5$	2.4	2500
CSB	449	0.72	27	0.10	1700
CLA	1392	0.294	10	0.62	1040

Table 1: ISOBIO materials properties at dry state at $T = 23^\circ\text{C}$

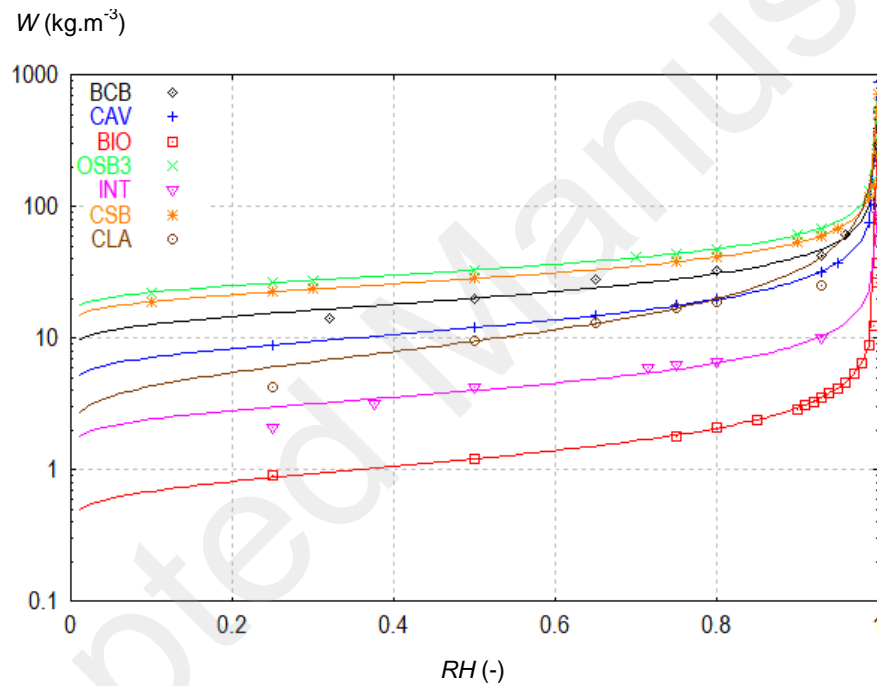


Figure 2: Isotherms of adsorption of the ISOBIO materials – Experimental data (symbols) and adjustments with the VG model

This VG model has been adjusted on the experimental data for each ISOBIO material. These adjustments have been performed to obtain the best possible correlations in the range of 40%-100%RH. The values of the adjustment coefficients are given in Table 2 and the Figure 2 shows the adjustments. Note that the maximum water contents W_{sat} have been considered equal to the measured porosities ε_0 multiplied by the liquid water density (*i.e.* 1000 kg.m^{-3}) excepted for BIO.

The evolutions of the vapor diffusion resistance factors μ as a function of the local water content w or RH have been ignored except for the Proclima INTELLO membrane because it is a hygrovariable material evolving very significantly as a function of RH . The data provided by Proclima/F-IBP have

been fitted by a logistic power as shown in Figure 3. Because of its great values, this parameter must be carefully modeled. Note that at 100% RH, μ decreases to 553.

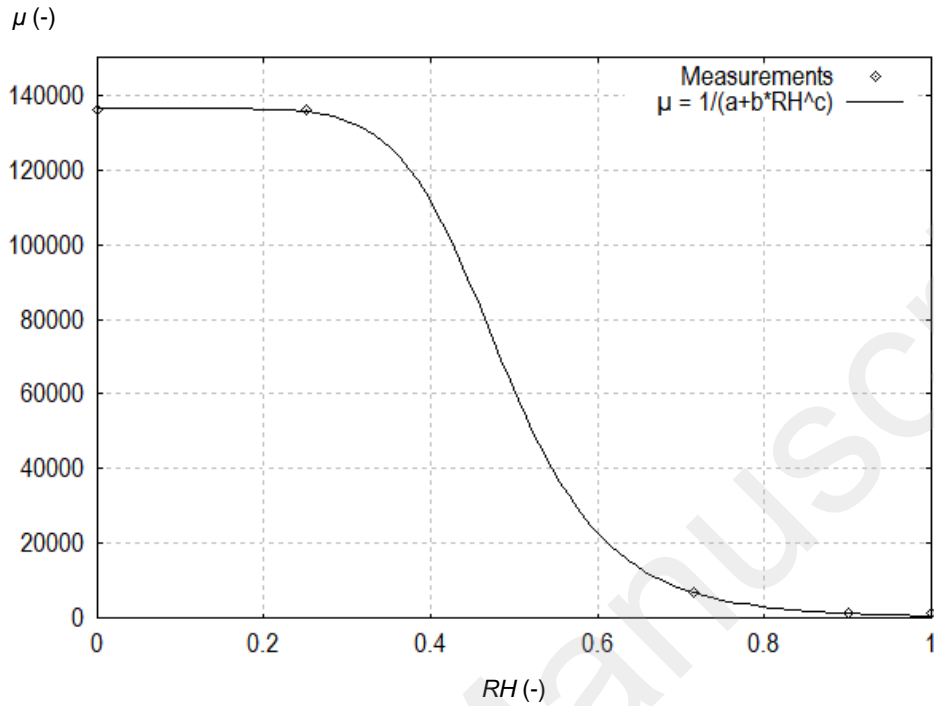


Figure 3: Vapor diffusion resistance factors μ of the Proclima INTELLO membrane as a function of RH – Measurements (points) and adjustment by a logistic power law – $a = 7.3310^{-6}$, $b = 1.8.10^{-3}$ and $c = 7.644$

Finally, the evolution of the thermal conductivities as a function of the water content has been modeled by the self-consistent scheme [16], which takes the following expression:

$$\lambda(W) = \lambda_s \left\{ 1 + \varepsilon_0 \left[(1 - \varepsilon_0) / 3 + \left(3 + (W / 1000 \varepsilon_0) (0.025 / 0.6 - 1) \right) \cdot \left(3(0.025 / \lambda_s - 1) - (W / 1000 \varepsilon_0) (0.025 / 0.6 - 1) (2 \cdot 0.6 / (\lambda_s + 1)) \right)^{-1} \right]^{-1} \right\} \quad (2)$$

The coefficient λ_s (which can be seen as the thermal conductivity of the material skeleton) have been adjusted such as $\lambda(W=0)$ equals λ_0 . The values of λ_s are given in Table 2.

	W_{sat} ($\text{kg} \cdot \text{m}^{-3}$)	h (-)	η (-)	λ_s ($\text{W} \cdot \text{m}^{-1} \cdot \text{K}^{-1}$)
BCB	546	8524	1.38	0.312
CAV	874	27490	1.435	0.53
BIO	348	228504	1.473	1.055
OSB3	609	11360	1.325	0.367
INT	85	2091	1.42	2.74
CSB	720	23172	1.334	0.38
CLA	294	271	1.656	0.995

Table 2: Adjustment coefficients – VG model and self-consistent scheme

2.3 Sensitivity study

Based on the materials thermal conductivities λ_0 and the vapor diffusion resistance factors μ_0 at dry state, the total thermal transmittance U and vapor resistance R of this wall are of $0.155 \text{ W.m}^{-2}.\text{K}^{-1}$ and $1.95.10^{11} \text{ Pa.m}^2.\text{s.kg}^{-1}$ respectively.

Then, by individually varying λ_0 and μ_0 of each layer ($\pm 10\%$), a sensitivity study has been performed. The sensitivities S_U and S_R given by eqs (3) and (4) of each layer are reported in Table 3. This means that if λ_0 or μ_0 is modified by $x\%$, U and R of the wall are modified by $x.S_U\%$ or $x.S_R\%$ respectively.

$$\begin{cases} S_U = \frac{U(\lambda_0 + 10\%) - U(\lambda_0 - 10\%)}{0.2U(\lambda_0)} \\ S_R = \frac{R(\mu_0 + 10\%) - R(\mu_0 - 10\%)}{0.2R(\mu_0)} \end{cases} \quad (3,4)$$

	S_U (-)	S_R (-)
BCB	0.03	0.01
CAV	0.115	0.027
BIO	0.77	0.03
OSB3	0.016	0.05
INT	0.0004	0.83
CSB	0.066	0.049
CLA	0.003	0.007

Table 3: Sensitivity study

Regarding U , the most sensitive material is obviously the Biofib Trio BIO (which is actually implemented in two layers of a total thickness of nearly 20 cm and which shows the lowest thermal conductivity) with a S_U of 0.77 and, to a much lesser extent, CAV and CSB.

Regarding R , the most sensitive material is obviously the membrane INT with a S_R of 0.83 and, to a much lesser extent, OSB3 and CSB. Note that the S_R of INT is given at dry state and will decrease very significantly with RH as this is a hygrovariable membrane.

Therefore, if the global characteristics of the ISOBIO reference wall need to be modified regarding any standard requirement, this sensitivity study can be of a precious help.

3 Mass transport governing equations

In this section, (i) air transport is ignored. In the porous samples, water is present in gaseous form (water vapor) and in liquid form. Therefore, there are two mass balance equations to consider. Assuming that (ii) the convective transport is negligible, they take the following form:

$$\begin{cases} \frac{\partial \bar{\rho}_v}{\partial t} - \nabla \cdot (D_{p,v} \nabla \bar{\rho}_v) = -R_s \\ \frac{\partial \bar{\rho}_l}{\partial t} - \nabla \cdot (D_{p,l} \nabla \bar{\rho}_l) = R_s \end{cases} \quad (5,6)$$

where $\bar{\rho}_v$ and $\bar{\rho}_l$ are the local water vapor and liquid water partial densities, $D_{p,v}$ and $D_{p,l}$ are the water vapor and liquid water diffusivities and R_s is the rate of sorption.

The local relative humidity can be expressed as follow:

$$\varphi = \frac{P_v}{P_{sat}} = \frac{\bar{\rho}_v RT}{M_w P_{sat}} \quad (7)$$

and the local liquid water partial density $\bar{\rho}_l$ (*i.e.* the local water content) will be written by convention as w . Thus, eqs (5,6) can be rewritten as follow:

$$\begin{cases} \frac{\partial (\varphi P_{sat})}{\partial t} - \nabla \cdot \left[\delta_{v,p} \frac{RT}{M_w} \nabla (\varphi P_{sat}) \right] = -\frac{RT}{M_w} R_s \\ \frac{\partial w}{\partial t} - \nabla \cdot (D_{p,l} \nabla w) = R_s \end{cases} \quad (8,9)$$

where the porous media vapor permeability $\delta_{v,p} = \delta_v / \mu = D_v M_w / \mu RT$, the water vapor diffusion resistance factor being given by: $\mu = \delta_v / \delta_{v,p} = D_v / D_{p,v}$.

It is commonly assumed that the rate of sorption R_s is very fast compared to the vapor diffusive flux leading to the so-called Künzel mass transfer equation [17].

Note that the coupling of eqs (8,9) with a hysteretic model (*e.g.* [4]) can easily be done: the reversal points (*i.e.* transitions between adsorption and desorption phases) are obtained when the sign of R_s changes.

As demonstrated and validated in the study of Reuge et al. [9] based on three different hemp concretes, the following expression for the sorption rate seems appropriate for the bio-based materials:

$$R_s = k_0 (w_{eq}(\varphi) - w)^2 \quad (10)$$

where k_0 is the local kinetic constant of sorption (adsorption or desorption) and w_{eq} is the equilibrium local water content given by the sorption isotherm at a local relative humidity φ . Note that this is a second order kinetics and consequently the unit of k_0 is expressed in $\text{day}^{-1}/(\text{kg} \cdot \text{m}^{-3})$. In [9], the values obtained for the studied hemp concretes are around $1 \text{ day}^{-1}/(\text{kg} \cdot \text{m}^{-3})$.

The classic heat transport governing equation is not given here but it is obviously taken into account considering latent heat of vaporization. At the wall surface, a convective heat transfer coefficient h_T is specified and the short-wave radiative flux is considered via an absorptivity coefficient α .

4. Determination of the kinetics constant of the ISOBIO materials

The time-dependent adsorption curves have been experimentally determined by gravimetric methods for CAV, BIO, OSB3 and CSB [14]. Regarding BCB, desorption experiments have been performed by an industrial partner (BCB). The characteristic diameter of the samples was of 4 cm.

If the sorption rate is slow compared to the vapor diffusive flux, the adjustments of 1D cylindrical calculations based on the local kinetics approach allow to determine the kinetic constant k_0 . According to Reuge et al. [9], k_0 should be constant in the range of 20% to 70% RH, for higher RH, k_0 tends to decrease because most of the sorption sites are already occupied. And actually, at RH higher than 80%, both local kinetics and diffusive mass transport are limiting phenomena [9]. Note that liquid diffusivity tends to usually initiate at RH of about 60% and becomes really significant from RH of about 80% as demonstrated in [18] and evidenced in the Fraunhofer Institute for Building Physics (FIBP) database. The 1D cylindrical calculations will be performed considering μ always equal to μ_0 (as a first step) and ignoring the liquid diffusivities.

4.1 CAVAC Rigid Panel

4.1.1 Experiments

Initially, the samples have been stabilized at a given ambient RH, and then the RH have been suddenly increased to a higher given value. For CAV, the following RH steps have been tested: 0-30%RH, 30-50%RH, 50-65%RH, 65-80% RH and 80-95% RH. Regarding the 0-30% RH and 50-65% RH steps, one of the samples was weighted continuously, for the other steps the samples were weighed discontinuously [14]. Four representative samples were used for each measurement, the differences were lower than 5%. The results of the measurements are shown in Figure 4: the stabilizations occur in more than 5 days. Note that regarding the 80-95% RH step, the measurements have been stopped before the stabilization because of initiation of mold development.

4.1.2 1D simulations

First, 1D simulations based of the Künzel approach have been performed: for the 0-30% RH, 30-50% RH, 50-65% RH steps, the times of stabilization are lower than 1 day and therefore greatly underestimated: this approach is invalidated (see Fig. 4 for the 30-50% RH step).

The adjustments of the 1D simulations based of the local kinetics approach leads to the following values of k_0 : 0.56, 0.3, 0.3, 0.12 and 0.08 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$ for the 0-30% RH, 30-50% RH, 50-65% RH, 65-80% RH and 80-95% RH steps respectively, as shown in Figure 4. Therefore, as expected, k_0 is the same for 30-50% RH and 50-65% RH steps (*i.e.* inside the range of 20% to 70% RH). The adjustments are globally very good with correlation coefficients greater than 0.99. However, note that the simulations and the values of k_0 obtained for the 65-80% RH and 80-95% RH steps can be unreliable since the liquid diffusivity is not taken into account. As noticed in [9] for hemp concretes, at moderate RH (< 80%), the limiting parameter is k_0 and the calculation is insensitive to μ_0 . At high RH, both the kinetics and diffusive mass transport have an effect on the global sorption rate.

4.2 Biofib Trio flexible

The adjustments of the 1D simulations based of the local kinetics approach on adsorption curves [14] leads to the following values of k_0 : 20, 9, 13 and 1.5 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$ for the 30-50% RH, 50-65% RH, 65-80% RH and 80-95% RH steps respectively (the 0-30% RH step measurements are too noisy to be exploited). Therefore, k_0 is around 14 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$ at common RH: this is a relatively high kinetic constant

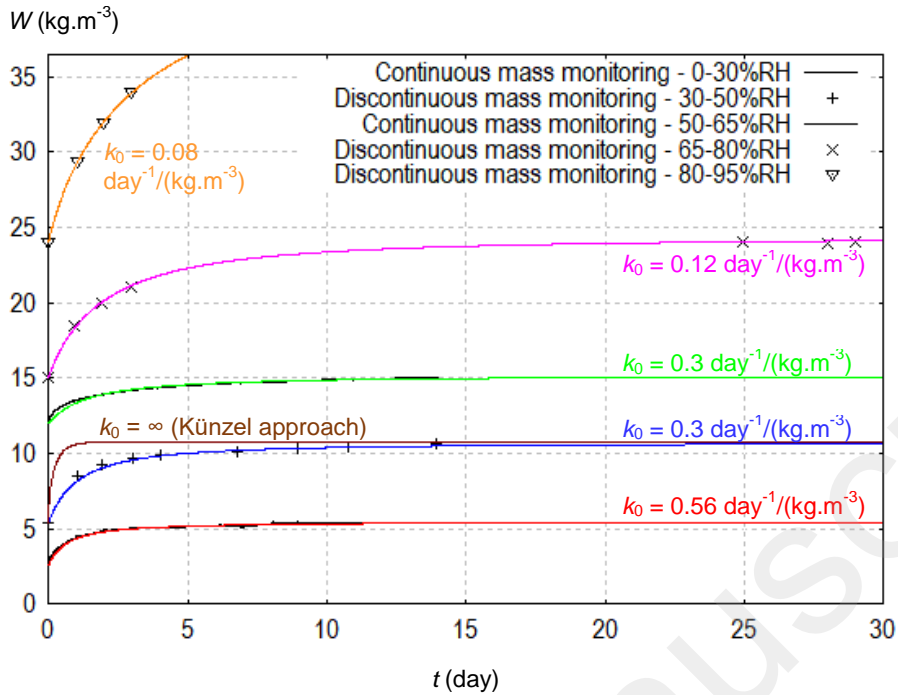


Figure 4: CAV sample – Adsorption measurements (symbols and black lines) – Adjusted 1D simulations (colored lines)

4.3 CSB Lignicell panel

This material is quite specific: it has a rather high μ_0 of 27 and both kinetics and diffusive mass transport are limiting. From 50% RH, both k_0 and μ have to be adjusted to obtain good agreements of the 1D simulations with the measurements. The adjustments showed in Figure 5 have been obtained with the following k_0 : 0.25, 0.25, 0.25, 0.01 and 0.001 $\text{day}^{-1}/(\text{kg.m}^{-3})$ and the following μ : 27 (*i.e.* μ_0), 27, 22, 8.5 and 8.5 for the 0-30%RH, 30-50%RH, 50-65%RH, 65-80%RH and 80-95%RH steps respectively. Note that the value of 8.5 corresponds the apparent μ "humid" measured by Collet et al. [14] at 53-88% RH.

4.4 OSB3

This material is also a particular case because its μ_0 of 138 is so high that diffusive mass transport is the only limiting phenomena. This does not mean that no local kinetics exists but that the local kinetics is fast compared to the diffusive fluxes. Consequently, the Künzel approach is justified in this case. Performing 1D simulations based on this approach, a good agreement is obtained with the measurements adjusting μ to the following values: 275, 100, 100, 40 and 10 for the 0-30%RH, 30-50%RH, 50-65%RH, 65-80%RH and 80-95%RH steps respectively. The results are shown in Figure 6.

Note that the μ_0 of 138 measured at 0-50% RH in [14] is indeed between 100 and 275 and that the measured μ "humid" (53-88% RH) of 45 [14] is close to the adjustment value of 40 for the 65-80%RH step.

Under these conditions, the kinetic constant cannot be determined.

4.5 BCB plaster

This material has been roughly studied by an industrial partner (BCB) in desorption conditions: 100-65% RH and 100-50% RH. The adjustments of the 1D simulations based of the local kinetics approach

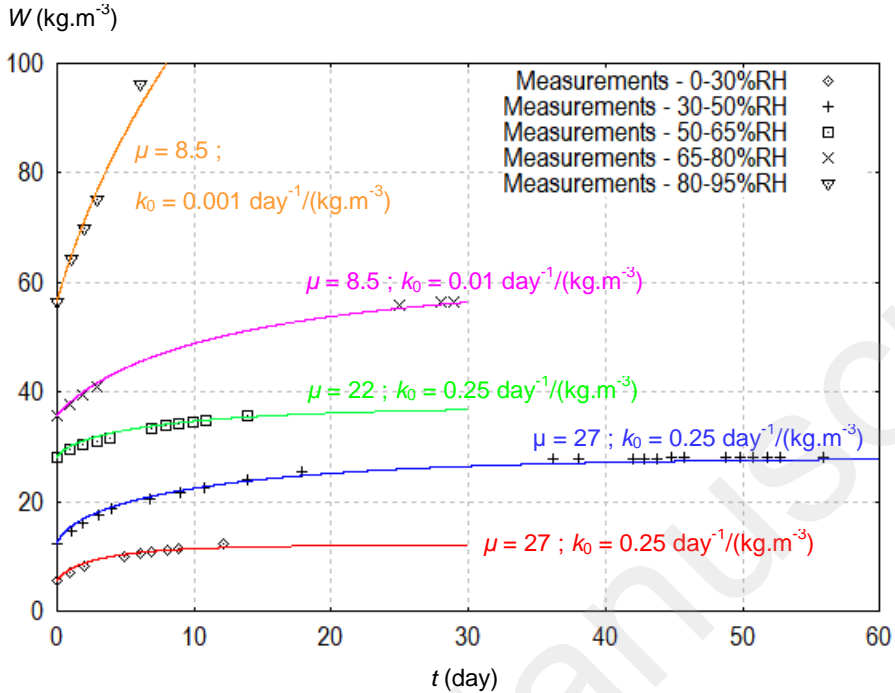


Figure 5: CSB sample – Adsorption measurements (symbols) – Adjusted 1D simulations (colored lines)

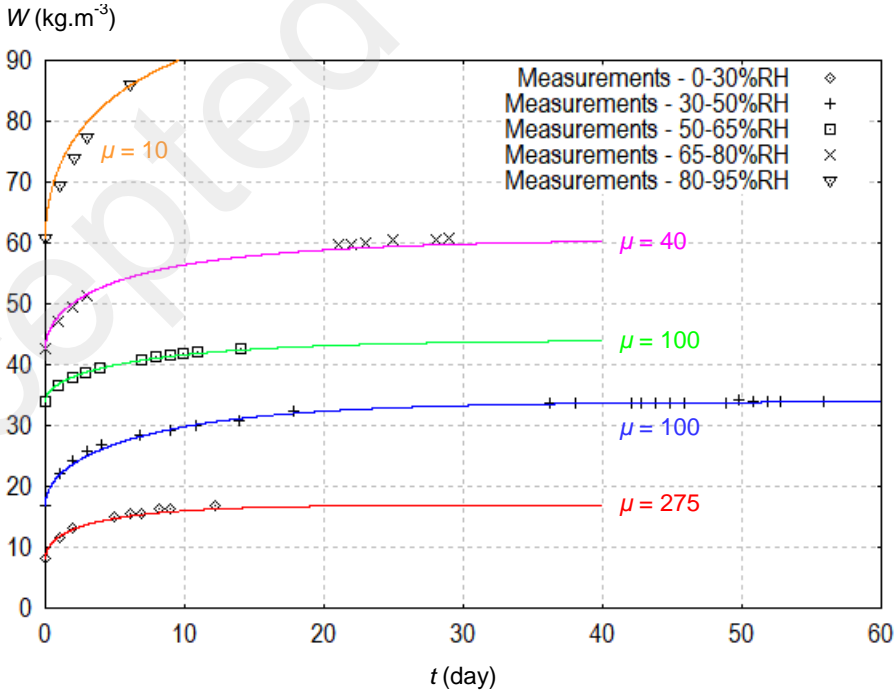


Figure 6: OSB3 sample – Adsorption measurements (symbols) – Adjusted 1D simulations (colored lines)

lead to the following values of k_0 : 0.0045 and 0.0055 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$ for the 100-65% RH and 100-50% RH steps respectively. Therefore, this is a quite slow kinetics constant of around 0.005 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$; note that from [9], the kinetic constants of adsorption and desorption are the same (at least for the three hemp concretes studied in the cited study).

4.6 Compilation of the kinetic constants

From this study, in the 20-70% RH range, the kinetics constants k_0 can be very different according to the material: from 0.005 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$ for BCB to about 14 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$ for BIO, *i.e.* a difference of almost 4 orders of magnitude. The values determined for RH greater than 80% are not reliable because the liquid diffusivities are unknown and have not been taken into account (see [9] for deeper explanations and investigations). For the simulations performed in the next section, the values of k_0 compiled in Table 4 will be considered. For the materials for which k_0 remains unknown, *i.e.* OSB3, INT and CLA, a median value of 0.25 $\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$ will be considered; note that the thicknesses of the layers of these three materials in the reference ISOBIO wall are relatively small, particularly INT with 0.25 mm thickness and note that the value of k_0 of CLA is of minor importance when the RH fluctuations at the indoor boundary conditions are almost non-existent (see section 5.2).

	k_0 ($\text{day}^{-1}/(\text{kg}\cdot\text{m}^{-3})$)
BCB	0.005
CAV	0.3
BIO	14
OSB3	0.25*
INT	0.25*
CSB	0.25
CLA	0.25*

*Unknown, median value

Table 4: ISOBIO materials kinetic constants k_0

The good adjustments of the calculations on the measured sorption curves is in themselves a self-consistent validation of the proposed kinetics approach. It should be emphasized that considering a kinetic order different from 2 would not lead at all to such good adjustments. And although lab-scale MBV (Moisture Buffer Value) test measurements had been performed in the framework of the ISOBIO project, at the moment they cannot serve as a second validation step of the kinetic approach for two reasons: for these experiments, (i) most hygric phenomena occur under the vicinity of the material surface and then are highly sensitive to the surface mass transfer coefficients which are extremely difficult to determinate precisely and (ii) by the fact that mass sample weight determinations (and then liquid content dynamics) are much less sensitive to the sorption kinetics than the relative humidity dynamics. Thus, the next part deals with in-situ RH measurements performed in a demonstrator: this is arguably the most consistent approach.

Note that for CAV and BIO, the analytical expression given in [9] allow to straightly estimate k_0 without the need of performing simulations.

5. Simulations of the HIVE demonstrator

In this final part, the hygrothermal behavior of the ISOBIO reference wall installed at the HIVE demonstrator (Wroughton, UK) is studied under the local climate during winter 2018. This consists in comparing the measurements and the simulations. To our knowledge, this is the first modeling work studying a multi-layered fully bio-based wall in real climatic conditions while various studies have already been carried out under controlled conditions and/or only one bio-based layer. Moujalled et al. [19] has studied the effect of real climatic conditions (Périgueux, FR) on a bio-based building with a wall of three layers: a hemp-lime concrete but with classic internal and external renders. Their simulations took into account the solar radiation and their results of the simulations were in globally good agreements with the measurements but the small time scale (on a few hours) *RH* dynamics was very notably underestimated. Piot et al. [20] has also studied a three-layered wall (Savoie, FR) in real climatic conditions: a hemp concrete but also with classic internal and external renders. Again, the calculated small time scale *RH* dynamics was very notably underestimated compared to the measurements. In [21, 22, 23, 24, 25, 26], the authors have studied the response of hemp concrete panels to controlled indoor and outdoor conditions. Even in these controlled operating conditions without solar radiation, most of these studies [21, 22, 26] lead to simulation results that underestimate clearly the small time scale *RH* dynamics. From that point of view, [23, 24, 25] seem to obtain better results playing on some parameters which have an effect on the hysteretic behavior of the sorption phenomena such as the initial water content (which is usually unknown) or the considered hysteretic model.

5.1 HIVE demonstrator: experimental setup

The ISOBIO test wall dimensions were 1.95mx1.95mx33.45cm. Inside the demonstrator, a CS215 SDI-12 Sensirion-based sensor was installed to measure air room *T* and *RH*. Heating equipment was used to maintain a constant indoor air temperature (BioGreen Phoenix electrical resistance heater with in-built air circulation fan). Outside the demonstrator, a weather station was installed to measure: *RH* and *T* (Rotronic HC2S3 sensor within 9-element ventilated solar shield), the wind speed (2-axis Gill Instruments Ultrasonic anemometer), precipitation (RM Young Tipping Bucket rain gauge) and horizontal global and diffuse solar radiation (Delta T Devices SPN1 Sunshine Pyranometer). Three *RH* and *T* sensors were installed inside the wall (CS215) at:

- position 1: CAV / BIO1 interface,
- position 2: BIO1 / OSB3 interface,
- position 3: INT / BIO2 interface.

In standard operating conditions, the accuracy of the CS215 SDI-12 Sensirion sensor measurements is of $\pm 2\%RH$ and $\pm 0.4^\circ C$ for *T*.

Figure 7 presents the external view of the ISOBIO wall panel under test at the HIVE test facility. At the center of the external face of the test panel, the external surface temperature is measurement using a thermistor encapsulated in an epoxy-filled aluminum housing clipped to the surface of the BCB render. This sensor is protected in a solar shielded and ventilated space. Offset from the center of the panel, the first of three embedded CS215 RHT sensors is fixed at the interface of CAV and BIO1, (*i.e.* position 1, approx. 75 mm from the external surface of the wall); the second CS215 RHT sensor is fixed at an approximate depth of 220 mm at the interface of BIO1 and the OSB3 board (position 2); and the third CS215 RHT sensor is at an approximate depth of 232 mm at the interface of the INT membrane and BIO2 (position 3). To avoid penetrations through the vapor control membrane,

cabling for sensors between the membrane and the outer face of the test wall are routed to the outside and those inboard of the membrane are routed to the interior of the test enclosure.



Figure 7: Outer face of the instrumented ISOBIO wall – HIVE demonstrator (Wroughton, UK)

5.2 Boundary conditions

The studied measurements have been performed during 18 days of winter 2018 (from 02/24 to 03/14), *i.e.* during 432 hours. During this period, the indoor and outdoor T and RH measurements are shown in Figures 8a and 8b respectively. As shown by these Figures, the climate was humid and cold, with outdoor RH varying between 50% and 100% and outdoor T varying between -7°C and 12°C . Solar short-wave radiation measurements are shown in Figure 9.

For the simulations, typical values have been considered for outdoor and indoor heat transfer coefficients, 17 and $8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-1}$ respectively [27, 28]. A value of 0.4 has been considered for the white wall render (BCB) absorptivity α in accordance with RT2012 French standards [29]. For outdoor and indoor mass transfer coefficients, typical values of $7.4\cdot 10^{-8}$ and $2.6\cdot 10^{-8} \text{ kg}\cdot\text{Pa}^{-1}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$ have been considered respectively [27, 28].

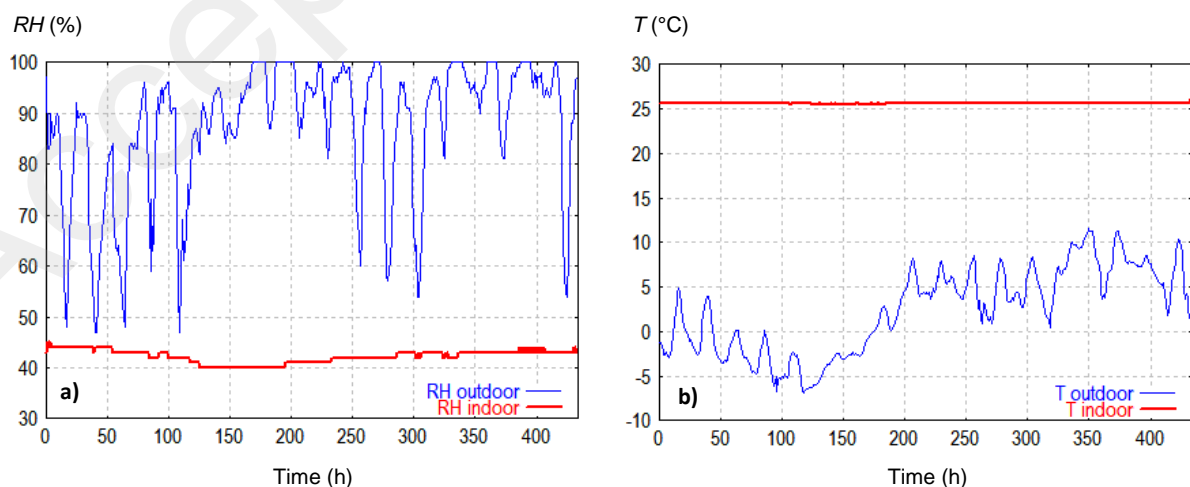


Figure 8: Indoor and outdoor RH (a) and T (b) measurements

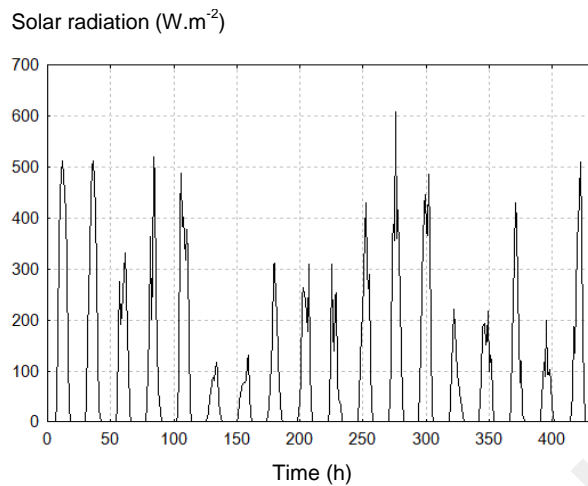


Figure 9: Solar short-wave radiation measurements

5.3 Simulation tools

Two simulation tools have been used:

- TMC, a home-made 1D Cartesian tool developed under Matlab based on the classic approach of Künzle,
- TMCKIN, a home-made 1D Cartesian tool developed under Matlab based on the local kinetics approach.

Note that TMC has been numerically validated on simple cases against WUFI™ 1D (a commercial tool) calculations.

5.4 Assumptions

For the mathematical models, assumptions are given in section 3.1. Regarding the sorption isotherms, the measurements done in adsorption conditions at 23°C (Fig. 2) were considered: consequently, no temperature effect or hysteresis phenomena were considered. Constant vapor resistance factor coefficients at dry state μ_0 were considered (Table 1) excepted for INT for which μ as a function of RH was considered (Fig. 3). Liquid diffusivities were neglected. The effects of wind and rain and long-wave radiation on outdoor boundary conditions were neglected for the simulations.

For TMCKIN simulations, kinetics constants k_0 given in Table 4 were considered. As clearly demonstrated in (Reuge, 2019), the actual values of k_0 and of the liquid diffusivities of the bio-based materials are strongly interdependent at high RH (>70-80%). Since the liquid diffusivities associated with the ISOBIO materials are unknown, the most reasonable approach is to consider the values of k_0 constant even at high RH .

5.5 Results of the simulations and discussion

The initial hygrothermal conditions in the wall have been chosen as follow:

- a constant RH of 80% in each layer,
- water contents w corresponding to RH of 80% according to the sorption isotherm in each layer,
- a constant temperature T of 10°C.

Obviously, these initial conditions do not correspond to the reality. Consequently, an iterative procedure has been used: the first simulations (with TMC and TMCKIN) have been performed over a full cycle of 18 days considering the aforementioned initial conditions. A second set of simulations have been run considering as initial conditions the final profiles of φ , w and T in each layer inside the wall. Finally, a third set of simulations have been run considering as initial conditions the final hygrothermal profiles of the second simulations in each layer. Only the results of this third set of simulations will be presented here. It worth noting that this procedure does not guarantee that the third simulations were run with exactly the good initial conditions but at least that they were more realistic than the aforementioned constant values used for the first simulations.

The results of the simulations (TMC and TMCKIN) are given at the aforementioned positions. Figures 10a, 11a and 12a show the measured and calculated RH over the full cycle (18 days) at pos. 1, 2 and 3 respectively. Figures 10b, 11b and 12b show the measured and calculated T at pos. 1, 2 and 3 respectively. Broadly, the RH obtained from the simulations are in good agreement with the measurements: the discrepancies are in a range of $\pm 4\%$. Regarding the temperature evolutions, the agreements are good provided the solar radiations is taken into account, the peaks of temperature corresponding to intense solar radiation periods are almost perfectly reproduced.

Then, it is particularly interesting to analyze the dynamics of the RH fluctuations at relatively small time scales (within at time interval of 24 h): at pos. 1 (Fig. 10a) and pos. 2 (Fig. 11a), they are patently underestimated by the TMC if the solar radiation is not taken into account and better but still largely underestimated predicted by TMC if the solar radiation is taken into account. The dynamics is better predicted when the solar radiation is considered because the temperature peaks resulting from the radiative flux increase the variations of water vapor saturation pressure and then of RH . The best agreements are obtained with TMCKIN: this is a straight effect of the local kinetics delaying adsorption / desorption of the water vapor, this is particularly observable at pos. 1 and pos. 2 (Fig. 10a and 11a). Extracting the main RH minima and maxima from the data, it is possible to estimate average RH variations: at pos1, they are of 2.8, 0.84, 1.4 and 3.2 respectively from the measurements, the TMC simulation without solar radiation, the TMC simulation and the TMCKIN simulation. Thus, the TMC simulation (with solar radiation) underpredicts the RH dynamics by 51% whereas the TMCKIN simulation slightly overpredict it by 12bb%. At this point, it must be reminded that the liquid water transport is ignored (because the liquid diffusivities are unknown for the studied materials) but its effect would undoubtedly soft the small time scale RH dynamics at such high RH of pos1. At pos2, the TMC simulation underpredicts the RH dynamics by 56% whereas the TMCKIN simulation slightly overpredict it by 16%. At pos3, the TMC simulation overpredicts the RH dynamics by 11% and the TMCKIN simulation by 31%: the overpredictions at this last position are questionable. The measured and predicted RH dynamics tend to be of a lesser extent at pos. 3 (Fig. 12a), this can be explained by the lesser effect of the solar radiation heat flux at such a deepness in the wall and by the filtering effect of the INT membrane on hygric variations.

Figure 13 shows the evolutions of local water content w as a function of local relative humidity φ at position 1 during the studied period of time (18 days) obtained with TMC and TMCKIN simulations. As expected, (φ, w) moves along the sorption isotherm of CAV according to TMC simulation whereas (φ, w) moves around it according to TMCKIN simulation. TMC simulation is always in an equilibrium

hygric state, TMCKIN simulation only from time to time. Broadly, with TMCKIN, ϕ evolves in a range of the equilibrium $\phi \pm 4\%$. Finally, as shown in Figure 14, the effect of consecutive cycles of the

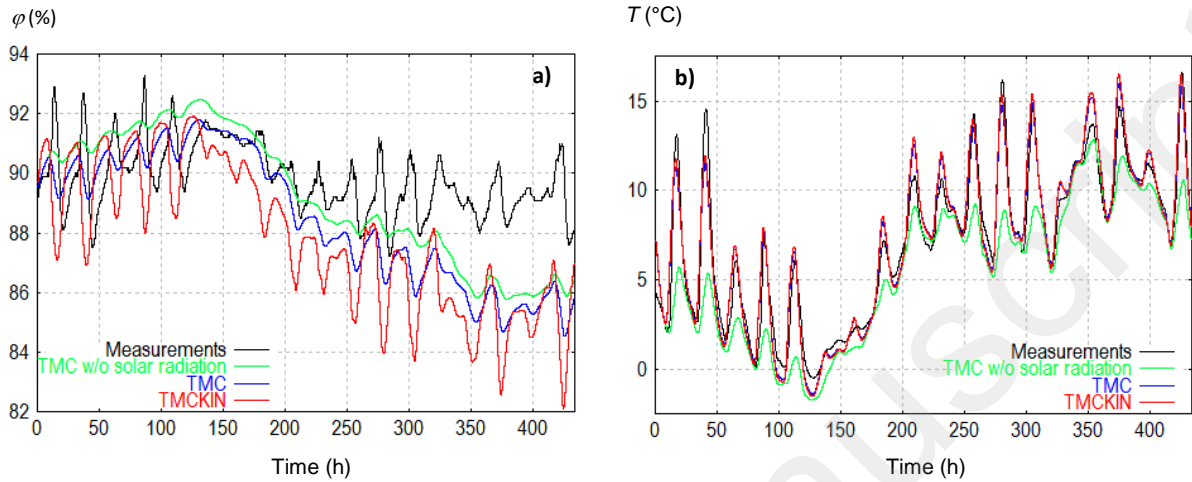


Figure 10: Measurements and simulations (TMC without solar radiation, TMC, TMCKIN) at position 1 – Temporal evolution of (a) relative humidity and (b) temperature

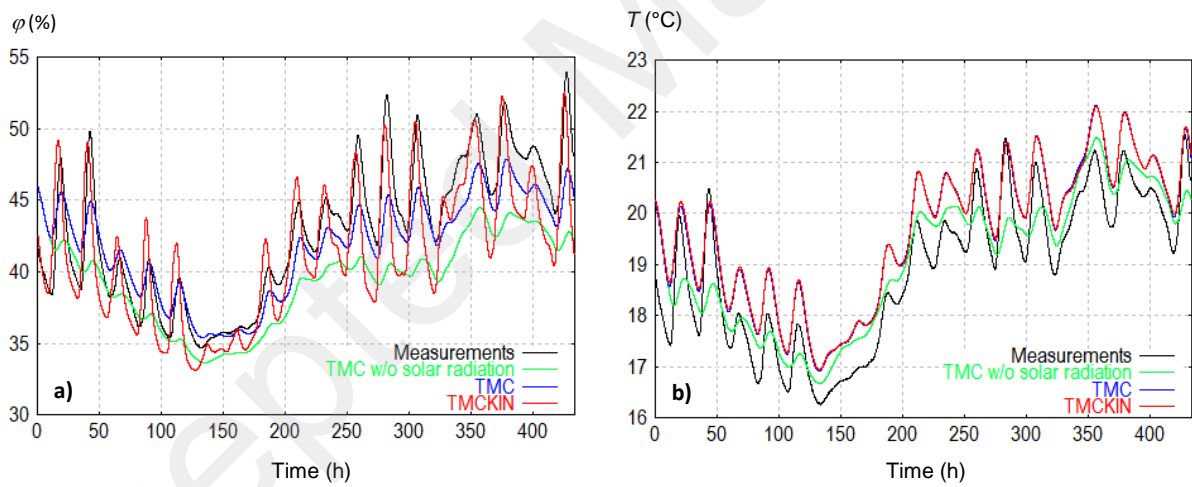


Figure 11: Measurements and simulations (TMC without solar radiation, TMC, TMCKIN) at position 2 – Temporal evolution of (a) relative humidity and (b) temperature

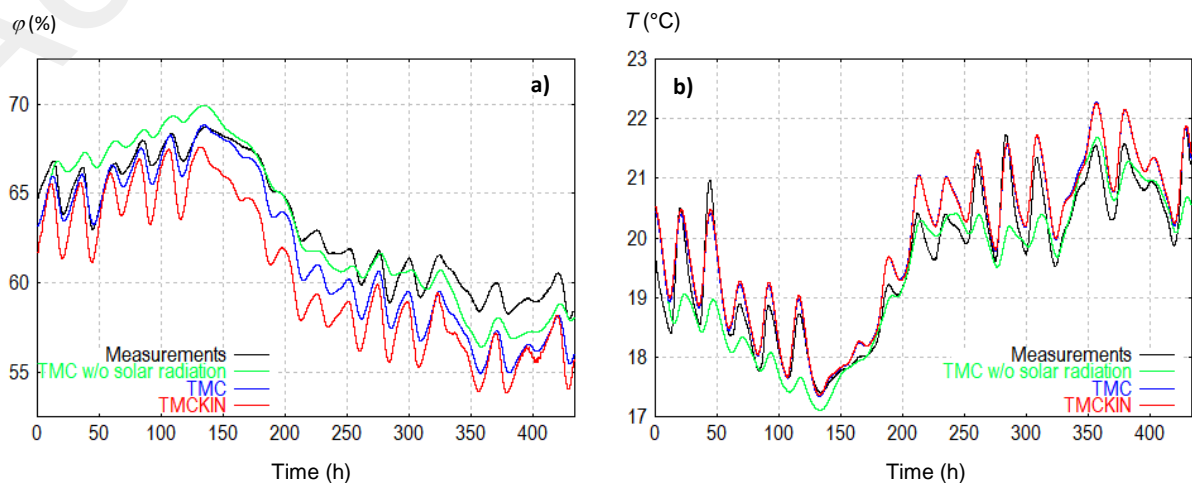


Figure 12: Measurements and simulations (TMC without solar radiation, TMC, TMCKIN) at position 3
 – Temporal evolution of (a) relative humidity and (b) temperature

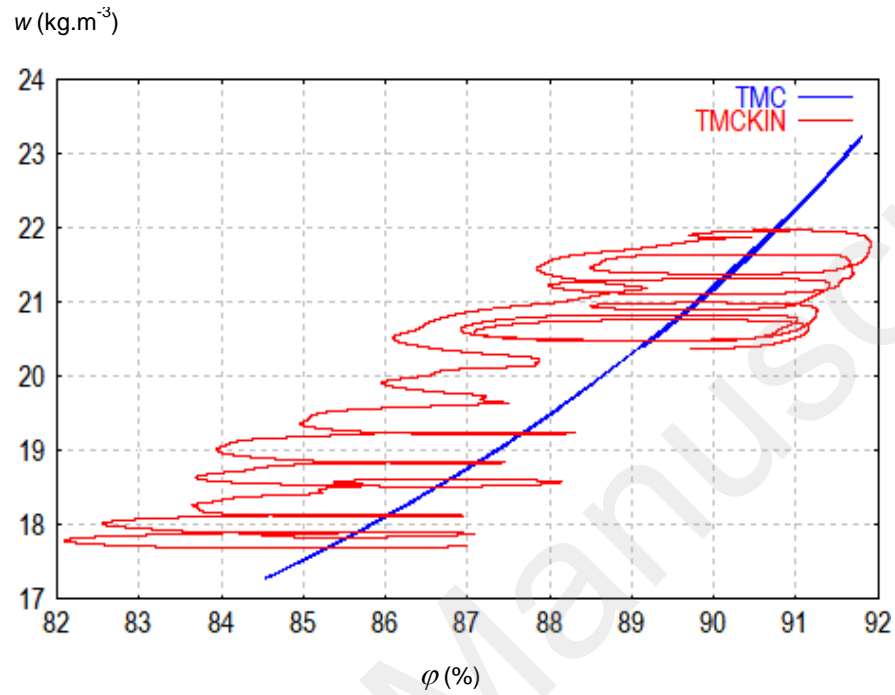


Figure 13: Evolution of local water content w as a function of local relative humidity ϕ at position 1 during the studied period of time (18 days) – TMC and TMCKIN simulations

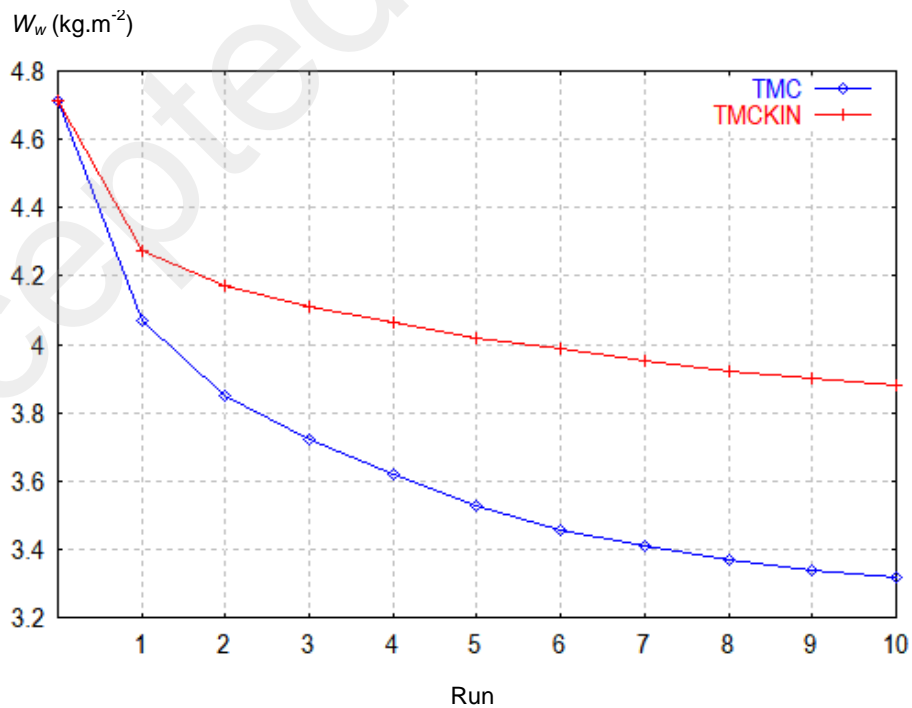


Figure 14: Total water content in the ISOBIO wall predicted after consecutive runs – TMC and TMCKIN simulations

considered 18 days is studied on the total wall water content considering every time the hygric state of the end of a run as initial conditions for the next run. This has been repeated 10 times with TMC and TMCKIN. Initially, the wall water content W_w is of 4.71 kg.m^{-2} . As aforementioned, the hygric state of the end of runs 2 had been considered as initial conditions for runs 3 which have been studied previously. From Fig. 14, the differences of W_w predicted with TMC and TMCKIN doesn't cease to increase run after run. At the end of run 10, the predicted total wall water contents W_w by TMC and TMCKIN are of 3.32 kg.m^{-2} and 3.88 kg.m^{-2} respectively, *i.e.* a difference as much as 17%. Thus, after a long period of time, the hygric states of the wall predicted by TMC and TMCKIN can be very significantly different. It deserves to be emphasized, for instance in the perspective of durability studies.

5.6 Sensitivity study

It seems interesting to study the sensitivity of various intrinsic properties of the studied materials on the small time scale RH fluctuations. The properties studied here are: the vapor resistance factor coefficient $\mu_0 \pm 20\%$, the kinetic constant $k_0 \pm 20\%$ and the thermal conductivity parameter $\lambda_s \pm 20\%$. At a given position, the average RH fluctuation obtained with TMCKIN is named $\overline{\Delta RH}$. The sensitivity S of a given properties, for instance μ_0 , on $\overline{\Delta RH}$ is given by:

$$S = \frac{\overline{\Delta RH}(\mu_0 + 20\%) - \overline{\Delta RH}(\mu_0 - 20\%)}{0.4\overline{\Delta RH}(\mu_0)} \quad (11)$$

This means that if μ_0 is modified by $x\%$, the predicted $\overline{\Delta RH}$ is modified by $x.S\%$ (at least in the range of $\mu_0 \pm 20\%$).

Three sensitivity studies have been performed:

- the first one varying the properties of the CAV layer,
- the second one varying the properties of the BIO1 and BIO2 layers,
- and the third one varying the properties of the INT layer.

For this last layer, only the μ_0 parameter was tested (the other properties of this very thin layer do not impact the results of the simulations).

The values of the sensitivities S , at pos1, pos2 and pos3, are reported in Table 5. Note that when the calculated S is lower than 0.01, a dash has been reported instead of a value.

From these results, it appears that the sensitivity S to the studied parameters is relatively low, *i.e.* taking into account the uncertainties given in Table 1, the effect on $\overline{\Delta RH}$ is relatively limited and does not put into question the considerations of the previous section. That being said, the most sensitive parameter for CAV and BIO1/BIO2 is μ_0 and therefore must be measured very carefully. For INT, variations of μ_0 in the $\pm 20\%$ range does not have any effect, its value remains anyway too high.

In further investigations, the effect of the slopes of the isotherms of sorption can be analyzed, but this parameter is straightly linked with the effects of the hysteresis phenomena which is outside the scope of the present study.

Studied layer: CAV			
	Pos1	Pos2	Pos3
μ_0	-0.304	0.014	-
k_0	-0.205	-	-
λ_s	0.194	0.127	0.159
Studied layers: BIO1 & BIO2			
μ_0	0.438	0.230	0.176
k_0	0.050	-0.139	-0.093
λ_s	-0.073	-0.028	0.084
Studied layer: INT			
μ_0	-	-	-

Table 5: Sensitivity study – Values of S (-)

6. Conclusion

This study has allowed to determine the kinetic constants of the key (on a hygric point of view) ISOBIO materials. According to these various materials, these kinetics constants can differ by four orders of magnitude. When the material vapor diffusion resistance factor μ_0 is too high (> 100 , *i.e.* OSB3), the kinetic constant cannot be determined by the proposed 1D numerical method.

The simulations of the HIVE demonstrator have been performed and compared to the measurements. This is the first modeling study of a multi-layered bio-based wall and, despite some assumptions, the simulations have led to overall good agreements with the measurements. Regarding the heat transfers, taking into account the solar radiation is required to obtain accurate agreements on temperature with the in-situ measurements. Regarding the hygric transfer, it has appeared that taking account both the solar radiation and the kinetics of sorption (TMCKIN) are required to reasonably predict the small time scale (less than 24 h) RH dynamics. In the perspective of simulations of RH variations inside a whole building, this work tends to show that the commercial simulation tools may fail to lead to reliable hygric results because they do not take into account the local kinetics effects.

In further investigations, the effects of an alternative climate and of internal RH loads on the ISOBIO reference wall will be studied. Moreover, alternative configurations of the ISOBIO wall will be investigated.

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