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Full paper

# Highly efficient and stable planar heterojunction solar cell based on sputtered and post-selenized $Sb_2Se_3$ thin film

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#### ABSTRACT

Antimony selenide (Sb<sub>2</sub>Se<sub>3</sub>) is regarded as one of the key alternative absorber materials for conventional thin film solar cells due to its excellent optical and electrical properties. Here, we proposed a Sb<sub>2</sub>Se<sub>3</sub> thin film solar cell fabricated using a two-step process magnetron sputtering followed by a post-selenization treatment, which enabled us to optimize the best quality of both the Sb<sub>2</sub>Se<sub>3</sub> thin film and the Sb<sub>2</sub>Se<sub>3</sub>/CdS heterojunction interface. By tuning the selenization parameters, a Sb<sub>2</sub>Se<sub>3</sub> thin film solar cell with high efficiency of 6.06% was achieved, the highest reported power conversion efficiency of sputtered Sb<sub>2</sub>Se<sub>3</sub> planar heterojunction solar cells. Moreover, our device presented an outstanding open circuit voltage ( $V_{OC}$ ) of 494 mV which is superior to those reported Sb<sub>2</sub>Se<sub>3</sub> solar cells. State and density of defects showed that proper selenization temperature could effectively passivate deep defects for the films and thus improve the device performance.

#### 1. Introduction

Thin film solar cells have made remarkable progress over the past few years as the power conversion efficiencies (PCE) of copper indium gallium selenide (CIGS) and cadmium telluride (CdTe) have reached over 22% [1,2]. However, the scarcity and toxicity of elements in these two solar cell systems could be problematic when it comes to large-area production in industry. Antimony selenide (Sb<sub>2</sub>Se<sub>3</sub>) is a promising alternative absorber material compared to the conventional thin film solar cells. Due to its outstanding properties such as simple crystal structure, ideal optical band gap (1.1-1.3 eV), high absorption coefficient  $(> 10^5 \text{ cm}^{-1})$  and considerable carrier mobility (~10  $cm^2V^{-1}s^{-1}$  [3–5],  $Sb_2Se_3$  has been regarded as one of the most attractive absorber candidates for the next-generation thin film solar cells. Nair et al. [6] firstly report Sb<sub>2</sub>Se<sub>3</sub> application in photovoltaic devices and generated a relatively low PCE of 0.66%. Sb<sub>2</sub>Se<sub>3</sub>-based thin film solar cells have been extensively studied since 2014 when Zhou et al. [7] achieved a 2.26% efficiency using a solution process. Thereafter, various techniques were utilized to fabricate  $\ensuremath{\text{Sb}_2\text{Se}_3\text{-}\text{based}}$  thin film solar cells. Tang's group extensively explored thermal evaporation

method [8–11] and 6% conversion efficiency was achieved for a ZnO/ $Sb_2Se_3$  superstrate configuration [12]. Further, a PCE of 7.6% was reported using vapor transport deposition (VTD) method to prepare highly [221]-oriented  $Sb_2Se_3$  thin film by Wen et al. [13].

Very recently, a PCE as high as 9.2% of Sb<sub>2</sub>Se<sub>3</sub> thin film solar cell with a core-shell structure (non-planar heterojunction) was reported by Li et al. [14]. [001]-oriented Sb<sub>2</sub>Se<sub>3</sub> nanorod arrays were successfully deposited onto Mo-coated glass using closed spaced sublimation (CSS) technique. A short circuit current density  $(J_{SC})$  over 30 mA/cm<sup>2</sup> has been obtained by effective carrier extractions along the Sb<sub>2</sub>Se<sub>3</sub> nanorods. The study demonstrated that the one-dimensional Sb<sub>2</sub>Se<sub>3</sub> nanorod arrays do improve the carrier transport, however, the surface roughness of the absorber as well as the space between nanorods have been significantly increased. This generates a potential problem for this structure as there is a risk that the conventional cadmium sulfide (CdS) film would contact the Mo-coated glass substrate, leading to shunt leakage formation and thus degrading the conversion efficiency of the device [14]. As a result, a thin TiO<sub>2</sub> film was introduced to the system by the author to optimize the coverage of CdS, which will undoubtedly, complicate the whole fabrication process of the device. Hence, although

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the nanorod array structure represents the highest efficiency of all  $Sb_2Se_3$  thin film solar cells by far, further investigation are required to fully understand the effectiveness of this particular configuration. On the other hand, planar heterojunction has been considered as the most appropriate structure for many thin film solar cells with high efficiencies such as CIGS, CdTe, CZTSSe and perovskite solar cell [15–18]. Moreover, given that apart from the reported nanorod array structure [14], all the other  $Sb_2Se_3$  thin film solar cells with high efficiency are based on planar heterojunction configuration. Therefore, it is vital to continue exploring new methods to fabricate high-quality planar heterojunction  $Sb_2Se_3$  thin film solar cells.

Magnetron sputtering is a well-established thin film deposition method that has been extensively used in absorber layer fabrication for CIGS and CZTS solar cells [19,20]. The method has the merits of easy control composition, excellent uniformity and simple experimental setup. Liang et al. [21] reported a PCE of 3.35% made by a radiofrequency (*RF*) magnetron sputtering method. Well-crystallized Sb<sub>2</sub>Se<sub>3</sub> thin film was prepared using *in-situ* sputtering technique at an optimized substrate temperature.

In this paper, a two-step process: *RF* magnetron sputtering deposition of amorphous Sb<sub>2</sub>Se<sub>3</sub> followed by a post selenization, was employed to achieve the best reported efficiency of sputtered Sb<sub>2</sub>Se<sub>3</sub> solar cells. By carefully optimizing the selenization procedure, highly crystallized [211]-oriented Sb<sub>2</sub>Se<sub>3</sub> ribbons and the Mo/Sb<sub>2</sub>Se<sub>3</sub>/CdS/ITO/Ag device with PCE of 6.06% were achieved, which is the highest conversion efficiency of sputtered Sb<sub>2</sub>Se<sub>3</sub> planar heterojunction solar cells. Besides, our device also presents a large open circuit voltage ( $V_{OC}$ ) of 494 mV which is higher than most of reported Sb<sub>2</sub>Se<sub>3</sub> thin film solar cell in literatures [4–14,22–24]. We have found that selenization temperature to be the key for the crystallinity, crystal orientation and chemical composition of the Sb<sub>2</sub>Se<sub>3</sub> films as well as the Sb<sub>2</sub>Se<sub>3</sub>/CdS planar heterojunction quality, and thus the conversion efficiency of the final device.

#### 2. Experimental detail

#### 2.1. Deposition of $Sb_2Se_3$ thin film

Sb<sub>2</sub>Se<sub>3</sub> thin films were deposited using radiofrequency (RF) magnetron sputtering deposition system. Sb<sub>2</sub>Se<sub>3</sub> powder with high purity (> 99.99%) were ball milled and sintered to prepare a dense Sb<sub>2</sub>Se<sub>3</sub> sputtering target. The XRD pattern of the Sb<sub>2</sub>Se<sub>3</sub> target is shown in Supplementary Fig. S1. Mo-coated glass substrates were subsequently cleaned in an ultrasonic bath using detergent, ethanol and deionized water before sputtering deposition. The background pressure of the sputtering vacuum chamber was evacuated below  $7.0 \times 10^{-4}$  Pa prior to the deposition. Ar gas flow rate was 40 sccm and the working pressure was kept at 1 Pa during the deposition process. The sputtering power and duration were selected to be 40 W and 90 min, respectively. There was no external heating during the deposition. As a result, amorphous Sb<sub>2</sub>Se<sub>3</sub> thin films with good homogeneity were obtained. Post-selenization process was subsequently carried out in order to better control the crystallization of the Sb<sub>2</sub>Se<sub>3</sub> films (the details of selenization process will be discussed later).

#### 2.2. Device fabrication

After the deposition and selenization of  $Sb_2Se_3$  thin films, CdS buffer layer was deposited onto the crystallized  $Sb_2Se_3$  films using chemical bath deposition (CBD). ITO window layer was magnetron sputtered after the deposition of CdS. The device surface was scribed into small squares with identical area by knife and Ag electrodes were deposited onto the ITO surface via thermal evaporation to form metallic contact. A substrate configuration of Mo/Sb\_2Se\_3/CdS/ITO/Ag was assembled for our Sb\_2Se\_3 solar cells. All the device efficiency characterizations of this work were based on active area of each device (0.15 cm<sup>2</sup>).

#### 2.3. Characterization of the Sb<sub>2</sub>Se<sub>3</sub> films and devices

X-ray diffraction (XRD, Ultima-iv,  $CuK_{\alpha}$  radiation under operation conditions of 40 kV and 40 mA from 10° to 60°) was utilized to investigate the crystal orientation of the Sb<sub>2</sub>Se<sub>3</sub> films. The surface and cross-sectional microstructures of the Sb<sub>2</sub>Se<sub>3</sub> films were characterized using a scanning electron microscope (SEM, SUPRA 55) and the chemical compositions of the films were analyzed using an energy dispersive X-ray spectroscope (EDS, BRUKER QUANTAX 200) equipped with the SEM. Transmission electron microscope (TEM) images were taken using a FEI Titan Cubed Themis G2 300 microscope. The sample for TEM imaging was prepared by ablating the thin film device using focused ion beam (FIB, FEI Scios). The band gap of the Sb<sub>2</sub>Se<sub>3</sub> film was measured using a LAMBDA 950 UV/VIS/NIR spectrophotometer. Ultraviolet photoelectron spectroscopy (UPS) measurement was performed using a Thermo Fisher ESCALAB 250Xi x-ray photoelectron spectrometer to determine the Fermi level and valance band of the Sb<sub>2</sub>Se<sub>3</sub> films. The current density-voltage (J-V) curves of the Sb<sub>2</sub>Se<sub>3</sub> devices were measured under 100 mW/cm<sup>2</sup> AM 1.5 G light illumination using a class AAA solar simulator at room temperature. The external quantum efficiency (EQE) spectra were measured using a Zolix SCS101 system and a Keithley 2400 source meter. Temperature-dependent  $V_{OC}$ measurements were carried out using a Lakeshore 325 temperature controller and the temperatures were swept from 350 K to 120 K in a step of 30 K. During the measurements, the devices were mounted inside a Janis VPF-100 cryostat and cooled with liquid nitrogen. Capacitance-voltage (C-V) measurements were conducted at AC amplitude of 30 mV and frequency of 10 kHz under a dark condition at room temperature. The DC bias voltage during the C-V measurements was applied from -1V to 0.3V. Drive level capacitance profiling (DLCP) measurements were performed with an AC amplitude from 20 mV to 140 mV and a DC bias voltage from -0.2 V to 0.2 V. Temperature-dependent capacitance-frequency (C-f-T) measurements were carried out within the frequency range of 1 kHz-10 MHz using the same cryostat and cooling system as mentioned above.

#### 3. Results and discussion

The schematic diagram of the Sb<sub>2</sub>Se<sub>3</sub> thin film preparation and the device fabrication is illustrated in Fig. 1. The full experimental details of magnetron sputtering and device fabrication have been provided in Experimental part. Herein, discussion will be mainly focused on the post-selenization step. After carefully controlling the sputtering parameters, amorphous Sb<sub>2</sub>Se<sub>3</sub> thin films with high uniformity were obtained. Subsequently, a post selenization process was carried out using a double-chamber vacuum tubular furnace (Fig. 1). The tubular furnace was evacuated to a relatively low background pressure using a mechanical pump before the selenization commenced, after that high purity Ar (> 99.999%) was pumped into the furnace and the working pressure was kept at  $5 \times 10^4$  Pa during the whole annealing process. 0.25 g of Selenium (Se) powder with high purity (> 99.999%) was kept at 400 °C during the selenization process whilst the temperature on the Sb<sub>2</sub>Se<sub>3</sub> thin film side increased from 340 °C to 460 °C in a step of 40 °C. Correspondingly, the samples annealed at different temperatures were denoted as 340-Sb<sub>2</sub>Se<sub>3</sub>, 380-Sb<sub>2</sub>Se<sub>3</sub>, 420-Sb<sub>2</sub>Se<sub>3</sub> and 460-Sb<sub>2</sub>Se<sub>3</sub>. The selenization duration was fixed at 20 min for each annealing scenario. Both the selenium temperature and the substrate temperature were raised at a ramping rate of 20 °C/min to the target temperature. The substrate was naturally cooled down to room temperature in the furnace after selenization.

Morphology and crystalline phases of  $Sb_2Se_3$  films annealed at various temperatures were shown in Fig. 2. From the XRD patterns, the overall diffraction peak intensities are increased with selenization temperature, suggesting crystallinity improvement of the  $Sb_2Se_3$  thin films upon annealing. However, the changes of the diffraction peak intensities are quite different, e.g. the (211), (221) and (002) peaks are

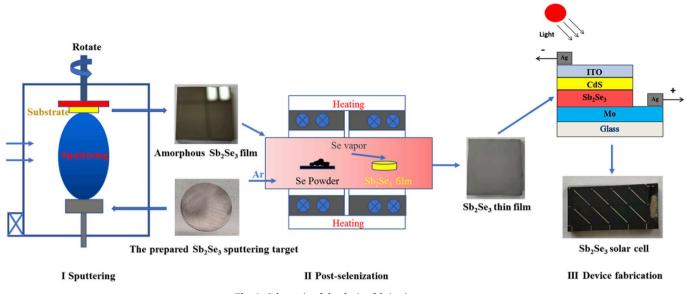


Fig. 1. Schematic of the device fabrication process.

increased sharply with selenization temperature, whereas those of the (120), (230) and (240) peaks decrease when selenization temperature was higher than 380 °C. Film texture has been reported as a key role in control of carrier transport [11]. In order to study the film orientation of  $Sb_2Se_3$  thin films quantitatively, texture coefficients (TC) of the diffraction peaks were calculated (Supplementary Fig. S2) based on the following equation [12]:

$$TChkl = \frac{I(hkl)}{I0(hkl)} / (\frac{1}{N} \sum_{i=1}^{N} \frac{I(h_i k_i l_i)}{I0(h_i k_i l_i)})$$
(1)

where  $I_{(hkl)}$  and  $I_{0(hkl)}$  are the diffraction peak intensities of (*hkl*) planes in the measured and standard XRD pattern of Sb<sub>2</sub>Se<sub>3</sub> (JCPDS 15–0861), respectively. Large TC value of a diffraction peak indicates preferred orientation along this particular direction [12]. The TC values of (hk0) planes of our samples tend to decrease with increasing selenization temperature in the range of 340–420 °C and then started to increase when the selenization temperature is further increased. Contrarily, the evolution of TC values of planes stacking vertically on the substrate, namely, (211), (221) and (002) planes showed an opposite trend, implying vertical orientation of our Sb<sub>2</sub>Se<sub>3</sub> thin film become dominant when the selenization was carried out at 420 °C.

The top-view images of Sb<sub>2</sub>Se<sub>3</sub> thin films annealed at different temperatures are shown in Fig. 2a, b, d and e (The surface SEM image of the as-deposited Sb<sub>2</sub>Se<sub>3</sub> thin film is given in Supplementary Fig. S3. It is featureless as expected, indicating the as-deposited Sb<sub>2</sub>Se<sub>3</sub> thin film is nearly amorphous). When the Sb<sub>2</sub>Se<sub>3</sub> film was annealed at 340 °C, the film was slightly crystallized as only tiny grains can be observed on the sample surface. For the sample annealed at 380 °C, larger Sb<sub>2</sub>Se<sub>3</sub> grains with size less than 200 nm were formed and distributed evenly over the sample surface. Much larger grains with size over 1  $\mu$ m can be observed

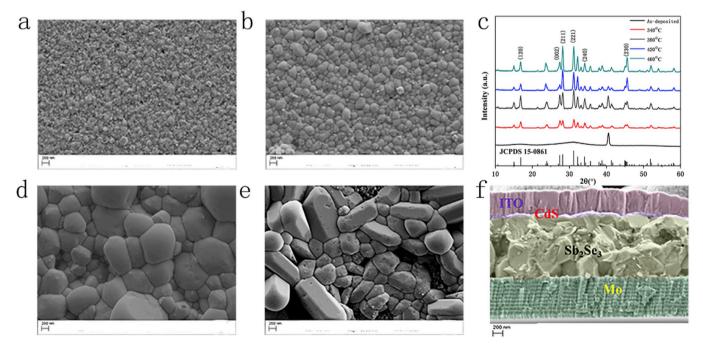


Fig. 2. Morphology evolution of Sb<sub>2</sub>Se<sub>3</sub> thin film. SEM top-view images of Sb<sub>2</sub>Se<sub>3</sub> thin films annealed at selenization temperatures of 340 °C (a), 380 °C (b), 420 °C (d) and 460 °C (e). XRD data of Sb<sub>2</sub>Se<sub>3</sub> thin films (c). SEM cross-sectional image of Sb<sub>2</sub>Se<sub>3</sub> thin film (final device) annealed at 420 °C (f).

 Table 1

 EDS results of Sb<sub>2</sub>Se<sub>2</sub> thin films annealed at various temperatures.

Samples	Sb (At%)	Se (At%)	Mo (At%)	Sb/Se
Sb <sub>2</sub> Se <sub>3</sub> target	40.34	59.66	N/A	0.676
As-deposited	41.34	57.78	0.88	0.715
340 °C	43.06	55.60	1.34	0.774
380 °C	41.83	56.37	1.80	0.742
420 °C	39.99	58.09	1.92	0.688
460 °C	35.12	57.67	7.21	0.609

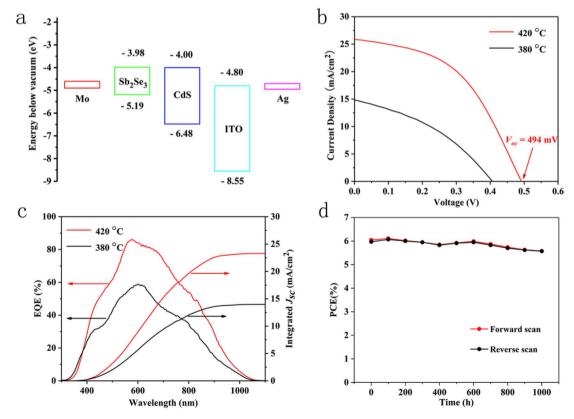
on the film surface once the selenization process was conducted at 420 °C. When the selenization temperature was as high as 460 °C, rodshaped Sb<sub>2</sub>Se<sub>3</sub> grains oriented in parallel with the substrate appeared, along with the formation of distinct micro-voids. This is consistent with our XRD data as the texture coefficients of the (hk0) peaks began to increase when selenization temperature was high than 420 °C.

The chemical composition results of the Sb<sub>2</sub>Se<sub>3</sub> thin films as well as the sputtering target analyzed by energy dispersive X-ray spectroscopy (EDS) are summarized in Table 1 (EDS patterns of Sb<sub>2</sub>Se<sub>3</sub> thin films annealed at various temperatures are shown in Supplementary Fig. S4). Sb<sub>2</sub>Se<sub>3</sub> thin films were Se-deficit (the ratios of Sb/Se were significantly higher than the stoichiometric composition of 0.66) when the selenization process was carried out below 400 °C probably due to high vapor pressure of Se. Under these circumstances, selenium vacancy defects could be dominant, affecting the performance of the device. It can be seen that optimal composition of our Sb<sub>2</sub>Se<sub>3</sub> thin films with a Sb/Se ratio of 0.688 could be obtained when selenization temperature was 420 °C. Annealing at 460 °C would turn the Sb<sub>2</sub>Se<sub>3</sub> film into Se rich as indicated by a Sb/Se ratio of 0.609. However, a high atomic percentage of molybdenum was also detected, suggesting partial decomposition of the thin films due to the excessive temperature. This is consistent with the SEM top-view image (Fig. 2e) as Mo-coated substrate can be directly observed due to the formation of micro-voids.

Overall, selenization temperature plays an important role in fabricating high-quality Sb<sub>2</sub>Se<sub>3</sub> films. Sb<sub>2</sub>Se<sub>3</sub> thin films prepared by RF magnetron sputtering were found to be optimum in terms of crystallinity, chemical composition and crystal orientation after annealed at 420 °C. Stoichiometric, vertically oriented Sb<sub>2</sub>Se<sub>3</sub> grains with size over 1  $\mu$ m have been successfully prepared under this particular selenization temperature, which is believed to be essential for carrier transport. Improper selenization temperatures would lead to insufficient crystallization or decomposition of the Sb<sub>2</sub>Se<sub>3</sub> films, making the films not suitable for device fabrication.

#### 4. Device performance

After the Sb<sub>2</sub>Se<sub>3</sub> absorber layer fabrication, CdS, ITO and front electrode were prepared in sequence to make the final device of Mo/ Sb<sub>2</sub>Se<sub>3</sub>/CdS/ITO/Ag in substrate configuration. The cross-sectional image of our complete champion device is displayed in Fig. 2f. Large Sb<sub>2</sub>Se<sub>3</sub> grains over 1 µm extending from the substrate to the CdS layer can be directly observed, implying the vertical growth of the Sb<sub>2</sub>Se<sub>3</sub> crystals. Decent interfacial adhesion is also evident by the compact and crack-free interfaces between individual layers. The valance band maximum (VBM) and conduction band minimum (CBM) of the Sb<sub>2</sub>Se<sub>3</sub> absorber layer that were obtained using ultraviolet photoelectron spectroscopy (UPS) and ultraviolet-visible spectroscopy (UV-VIS) techniques are -5.19 eV and -3.98 eV, respectively (Supplementary Fig. S5), whereas the energy levels of CdS and ITO were obtained from the literature [25]. The band alignment diagram of our device is illustrated in Fig. 3a. It can be easily seen that flow of photogenerated electrons from Sb<sub>2</sub>Se<sub>3</sub> to ITO could be significantly facilitated due to the optimized band alignment of the device. Besides, considerable VBM



**Fig. 3. Device performance**. Band alignment diagram of the Sb<sub>2</sub>Se<sub>3</sub> device (**a**). Current density-voltage (J–V) curves (**b**) and external quantum efficiency (EQE) and integrated  $J_{SC}$  (**c**) of 380-Sb<sub>2</sub>Se<sub>3</sub> and 420-Sb<sub>2</sub>Se<sub>3</sub> devices (**c**). Device stability of the 420-Sb<sub>2</sub>Se<sub>3</sub> device after 1000 h storage in air ambient without special treatment/ encapsulation (**d**).

offset also makes CdS an effective hole blocking layer which helps to reduce recombination in the device. Since the Sb<sub>2</sub>Se<sub>3</sub> films annealed at 340 °C and 460 °C were poorly crystallized and partially decomposed, the devices made from these films barely have any conversion efficiency. Therefore, discussion of device performance will be limited to the 380-Sb<sub>2</sub>Se<sub>3</sub> and 420-Sb<sub>2</sub>Se<sub>3</sub> devices and the results are shown in Fig. 3b–d.

Device performance tested under AM 1.5 G light illumination showed a PCE of 6.06% for 420-Sb<sub>2</sub>Se<sub>3</sub> device,  $J_{SC}$  of 25.91 mA/cm<sup>2</sup>,  $V_{OC}$  of 494 mV and fill factor (FF) of 47.73%, whilst the corresponding parameters for the 380-Sb<sub>2</sub>Se<sub>3</sub> device are 2.26%, 14.81 mA/cm<sup>2</sup>, 407 mV and 38.1%, respectively (Fig. 3b and Supplementary Table S1). 100 devices for each sample category were tested to study the reproducibility of the devices and the main parameter boxplots of the two categories are illustrated in Supplementary Fig. S6. The external quantum efficiency (EQE) of these two devices are given in Fig. 3c, obviously the photo-response of the 420-Sb<sub>2</sub>Se<sub>3</sub> device is much stronger than that of the 380-Sb<sub>2</sub>Se<sub>3</sub> device over the most of the region. The best device presents EQE values over 80% from 550 to 700 nm, whereas the maximum EQE of the 380-Sb<sub>2</sub>Se<sub>3</sub> device is below 60% for the whole region. In summary, the device performance of the 420-Sb<sub>2</sub>Se<sub>3</sub> device is superior to that of 380-Sb<sub>2</sub>Se<sub>3</sub> device. We attribute this to the optimized orientation and crystallinity of the 420-Sb<sub>2</sub>Se<sub>3</sub> thin film. XRD results have demonstrated that annealing at 420 °C significantly induced the growth of vertical oriented grains (mainly [221], [211] and [002] orientation) for the Sb<sub>2</sub>Se<sub>3</sub> films, which are believed to have fewer dangling bonds and recombination centers at the grain boundaries [11]. As a result, recombination losses would be minimized and an optimized heterojunction quality could be obtained in the 420-Sb<sub>2</sub>Se<sub>3</sub> device. In contrast, Sb<sub>2</sub>Se<sub>3</sub> grains have shown orientations in parallel with the substrate surface when annealed at 380 °C and dangling-bond-rich grain boundaries will be produced in this case thus leading to a relatively poor adhesion at the Sb<sub>2</sub>Se<sub>3</sub>/CdS interface. In addition, much larger grain size in the 420-Sb<sub>2</sub>Se<sub>3</sub> device could effectively suppress recombination losses at the grain boundaries further, leading to higher  $V_{OC}$  and FF. Moreover, studies have reported that it is much easier for charge carriers to transport through [221] or [211] oriented grains than through [120] oriented grains [11], which is evidenced by the much higher J<sub>SC</sub> of our 420-Sb<sub>2</sub>Se<sub>3</sub> device.

Current density-voltage measurement was also undertaken for our champion device using different scanning directions (Supplementary Fig. S7). A hysteresis-free performance is clearly seen as two curves are overlapped with each other. In order to study the device stability, the device was stored in air ambient without any special treatment/encapsulation for over 1000 h. Device efficiency was tested every 100 h and the result is shown in Fig. 3d. The PCE of our best device was maintained at relatively high levels throughout the whole test and a final PCE of 5.58% (only a small decay of around 9%) was achieved, indicating an excellent stability of our device.

In order to further characterize the morphology and configurational properties of the devices, the champion device was ablated using focused ion beam and cross-sectional TEM image of the device is presented in Fig. 4a. Apparently individual layers including molybdenum substrate, CdS and ITO could be well distinguished. A MoSe<sub>2</sub> film could be found between the Mo and Sb<sub>2</sub>Se<sub>3</sub> layers which is possibly formed due to high temperature selenization. Such a MoSe<sub>2</sub> layer was deliberately introduced into the system prior to Sb<sub>2</sub>Se<sub>3</sub> deposition to improve the back contact for Sb<sub>2</sub>Se<sub>3</sub> thin film solar cells in substrate configuration, has also been reported by Li et al. [26]. However, the effect of this MoSe<sub>2</sub> layer in our case is not fully understand and needs for further investigation. Three arbitrary spots a, b and c were selected for high-resolution transmission electron microscopy (HRTEM) imaging around the top, middle and bottom regions of the Sb<sub>2</sub>Se<sub>3</sub> absorber layer to examine the grain continuity across the whole film. Lattice fringes of the three spots are shown in Fig. 4b-d and the distances between lattice lines of all three spots were measured to be 0.318 nm, 0.319 nm and 0.318 nm, respectively. This reveals the excellent continuity of the Sb<sub>2</sub>Se<sub>3</sub> grain along the Y-axis direction as all the distances between lattice lines for the three spots are identical which correspond to the (211) planes in orthorhombic Sb<sub>2</sub>Se<sub>3</sub>. The high consistency of crystal orientation across the whole Sb<sub>2</sub>Se<sub>3</sub> film is beneficial for charge carrier transport and thus efficiency improvement [11].

High-angle annular dark-field scanning transmission electron microscope (HAADF-STEM) equipped with energy dispersive spectroscopy (EDS) characterization was further carried out to study the elemental distribution of the device. The red arrow in Fig. 4a indicates the EDS line scan direction. Elemental profiles and elemental mapping of the device are illustrated in Fig. 4e and f, respectively. Elemental

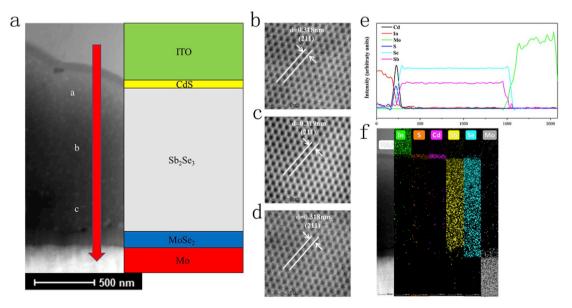


Fig. 4. TEM characterization of the Sb<sub>2</sub>Se<sub>3</sub> champion device. Cross-sectional TEM image of the Sb<sub>2</sub>Se<sub>3</sub> champion device. The red arrow indicates the EDS line scan direction of the elemental mapping for the device (a) Lattice fringes of three arbitrary spots a, b and c across the Sb<sub>2</sub>Se<sub>3</sub> thin film in (a) performed by HRTEM are given in (b), (c) and (d), correspondingly. EDS elemental profiles (e), HAADF-STEM image and EDS elemental mapping (f) of the device. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

distribution with good uniformity of Se and Sb could be clearly observed throughout the whole Sb<sub>2</sub>Se<sub>3</sub> layer. Crossovers of different elemental distribution profiles were found at both ends of the Sb<sub>2</sub>Se<sub>3</sub> layer, implying occurrence of elemental inter-diffusion at both the Mo/Sb<sub>2</sub>Se<sub>3</sub> and Sb<sub>2</sub>Se<sub>3</sub>/CdS junctions. Since heterojunction interfaces between the absorber layer and buffer layer always play a crucial role in device performance for thin film solar cells, here we will focus our discussion on elemental inter-diffusion at the Sb<sub>2</sub>Se<sub>3</sub>/CdS heterojunction interfaces. HRTEM images as well as EDS elemental mapping of the Sb<sub>2</sub>Se<sub>3</sub>/ CdS interface are presented in Supplementary Fig. S8. No abrupt interfacial boundary is observed between the Sb<sub>2</sub>Se<sub>3</sub> and CdS layers (Supplementary Fig. S8(b)), suggesting good adhesion at the heterojunction interface. For EDS elemental mapping results (Supplementary Fig. S8(c)), elemental inter-diffusions can be observed for all the four elements, i.e. Sb, Se, Cd and S. Such elemental inter-diffusion phenomenon was reported to be essential for favorable band alignment formation and reduction of recombination at the heterojunction interfaces [20]. However, on the other hand, Wang et al. reported that a strong interfacial intermixing, especially over-diffusion of Cd might deteriorate the device performance [12]. Therefore, the full effect of elemental inter-diffusion at the heterojunction interface on device performance for thin film solar cells has not been fully understood yet and future investigations are urgently required for this particular area.

Based on literature, efficiency records of planar heterojunction Sb<sub>2</sub>Se<sub>3</sub> thin film solar cells fabricated by various techniques are summarized in Table 2. Compared with Liang's report [21], a nearly 3% efficiency improvement for Sb<sub>2</sub>Se<sub>3</sub> solar cell prepared by magnetron sputtering has been achieved in this work. More importantly, our best Sb<sub>2</sub>Se<sub>3</sub> solar cell with a conversion efficiency of 6.06% via RF magnetron sputtering represents the highest PCE of all sputtered Sb<sub>2</sub>Se<sub>3</sub> planar heterojunction solar cells so far. We attribute this to the additional selenization process which not only compensates for the selenium loss during the sputtering process, but also produce better crystallinity and orientation for the Sb<sub>2</sub>Se<sub>3</sub> films. It should be also noted that a large value of open circuit voltage  $V_{OC}$  of 494 mV has been achieved, which is higher than any other reported pure Sb<sub>2</sub>Se<sub>3</sub> thin film solar cell [4-14,22-24], has been provided by our champion device. A decent short circuit current density  $J_{SC}$  of 25.91 mA/cm<sup>2</sup> of our device is comparable to that of state of the art Sb<sub>2</sub>Se<sub>3</sub> solar cells as well. However, the fill factor (FF) of our device (47.7%) is relatively low compared to other representative devices in the table. The poor FF is probably due to the unoptimized interface between the Sb<sub>2</sub>Se<sub>3</sub> thin film and Mo contact. As mentioned before, a thick layer of MoSe<sub>2</sub> (~200 nm) could be directly observed from the TEM image of the Sb<sub>2</sub>Se<sub>3</sub> device (Fig. 4a). Considering the thickness of MoSe<sub>2</sub> layer was only several tens of nanometers in other reports that focused on MoSe<sub>2</sub> optimization [26], the over thick MoSe<sub>2</sub> layer in this work might increase the series resistance  $R_S$  of the device, leading to FF attenuation.

#### 5. Interface characterization of devices

In order to analyze the interfacial properties of the devices, temperature-dependent open circuit voltage ( $V_{OC}$ -T) measurements were carried out from 350 K to 120 K. Activation energy of recombination activity within the devices can be obtained by extrapolating  $V_{OC}$  to the *Y*-axis (Fig. 5a) [12]. The obtained valuer of activation energy for the 420-Sb<sub>2</sub>Se<sub>3</sub> device is 1.13 eV, which is very close to the band gap of our Sb<sub>2</sub>Se<sub>3</sub> films (1.21 eV), whereas the activation energy of the 380-Sb<sub>2</sub>Se<sub>3</sub> device is only 1.06 eV. This implies that interfacial recombination is more prominent for the 380-Sb<sub>2</sub>Se<sub>3</sub> device than that for 420-Sb<sub>2</sub>Se<sub>3</sub> device [12], mainly due to poor adhesion at the Sb<sub>2</sub>Se<sub>3</sub>/CdS interface originated from dangling-bond-rich grain boundaries of the 380-Sb<sub>2</sub>Se<sub>3</sub> device.

Capacitance-voltage (*C*–*V*) profiling and deep-level capacitance profiling (*DLCP*) were further conducted to characterize interfacial defects of the devices (Fig. 5b). According to literature [13], the interfacial defect density can be derived from the difference between *C*–*V* measured doping density ( $N_{C-V}$ ) and *DLCP* measured doping density ( $N_{DLCP}$ ) where  $N_{C-V}$  represents responses from free carriers, bulk defects and interfacial defects, while  $N_{DLCP}$  only reflects responses from free carriers and bulk defects. The plots of  $N_{C-V}$  and  $N_{DLCP}$  against the profiling depth *x* can be calculated according to the following equation:

$$N_{C-V} = \frac{-2\varepsilon_{r,n}N_D}{\left(\frac{d(1/C^2)}{dV}\right)qA^2\varepsilon_{0}\varepsilon_{r,n}\varepsilon_{r,p}N_D + 2\varepsilon_{r,p}}$$

$$\{N_{DLCP} = -\frac{C_0^3}{2q\varepsilon_{0}\varepsilon_{r,p}A^2C_1}$$

$$x = \varepsilon_0\varepsilon_{r,p}A/C_0$$
(2)

where  $N_D$  is the doping density of CdS, A is the device area,  $\varepsilon_{r,n}$  and  $\varepsilon_{r,p}$ are the relative permittivity of CdS and  $Sb_2Se_3$ , respectively,  $C_0$  and  $C_1$ are two quadratic fitting parameters derived from the C-V curves. It can be clearly seen that the difference between  $N_{C-V}$  and  $N_{DLCP}$  of the 420-Sb<sub>2</sub>Se<sub>3</sub> device is much smaller than that of the 380-Sb<sub>2</sub>Se<sub>3</sub> device, suggesting lower defect density and recombination loss at the Sb<sub>2</sub>Se<sub>3</sub>/ CdS interface for the 420-Sb<sub>2</sub>Se<sub>3</sub> device. In the region of Sb<sub>2</sub>Se<sub>3</sub>/CdS heterojunction interface, nearly the whole depletion width  $(W_d)$  is located within  $Sb_2Se_3$  layer since the doping density of  $Sb_2Se_3$  is much lower than that of CdS, as a result, the volume to surface ratio is  $W_d$  and interfacial defect densities for 420-Sb<sub>2</sub>Se<sub>3</sub> and 380-Sb<sub>2</sub>Se<sub>3</sub> devices could be calculated as  $1.88 \times 10^{11}$  cm<sup>-2</sup> and  $1.64 \times 10^{12}$  cm<sup>-2</sup>, respectively. It should be noted that the interfacial defect density of our best cell is comparable to that of  $Sb_2Se_3$  solar cells with a high efficiency [12], which yields far superior  $V_{OC}$  and FF compared with the 380-Sb<sub>2</sub>Se<sub>3</sub> device.

 $C^{-2}$ -*V* curves were also plotted to calculate the built-in voltage (*V*<sub>bi</sub>) for the two devices (Fig. 5c). The curves were linearly fitted and the

Table 2

Summary of planar heterojunction Sb<sub>2</sub>Se<sub>3</sub> solar cell publications by different fabrication methods.

Method	Device configuration	<i>Eff</i> (%)	$V_{oc}$ (mV)	$J_{ac}$ (mA/cm <sup>2</sup> )	FF (%)	Ref.
Solution	FTO/TiO2/CdS/Sb2Se3/Spiro/Au	3.9	340	27.2	41.9	Chen [27]
Co-eva <sup>a)</sup>	Glass/Mo/Sb <sub>2</sub> Se <sub>3</sub> /CdS/ZnO/AZO/Ag	4.25	427	17.11	58.15	Mai [26]
RTE <sup>b)</sup>	ITO/CdS/Sb <sub>2</sub> Se <sub>3</sub> /Au	7.04	413	28.7	59.3	Tang [24]
VTD <sup>c)</sup>	ITO/CdS/Sb <sub>2</sub> Se <sub>3</sub> /Au	7.6	420	29.9	60.4	Tang [13]
CSS <sup>d)</sup>	FTO/CdS/Sb <sub>2</sub> Se <sub>3</sub> /Au	6.84	421	28.4	57.1	Tang [28]
CSS <sup>d)</sup>	Glass/Mo/Sb <sub>2</sub> Se <sub>3</sub> /Cd <sub>x</sub> Zn <sub>1-x</sub> S/ZnO/ZnO:Al	6.71	403	25.69	64.78	Mai [29]
Sput <sup>e)</sup>	Glass/Mo/Sb <sub>2</sub> Se <sub>3</sub> /CdS/ZnO/AZO/Ag	3.35	437	15.93	48	Liang [21]
Sput-Se <sup>f)</sup>	Glass/Mo/Sb <sub>2</sub> Se <sub>3</sub> /CdS/ITO/Ag	6.06	494	25.91	47.7	This work

<sup>a</sup> Co-evaporation.

<sup>b</sup> Rapid thermal evaporation.

<sup>c</sup> Vapor transport deposition.

<sup>d</sup> Closed space sublimation.

<sup>e</sup> Magnetron sputtering deposition.

<sup>f</sup> Magnetron sputtering deposition and post-selenization.

value of  $V_{bi}$  were determined from the *x*-intercept. Compared with the 380-Sb<sub>2</sub>Se<sub>3</sub> device, a sharp  $V_{bi}$  increase of 179 mV has been observed for the 420-Sb<sub>2</sub>Se<sub>3</sub> device, which is attributed to the greatly improved Sb<sub>2</sub>Se<sub>3</sub>/CdS interface. As mentioned before, the  $V_{OC}$  of our best device (494 mV) is one of the highest values among the state of the art Sb<sub>2</sub>Se<sub>3</sub> thin film solar cells prepared by different methods. On the other hand, the  $V_{bi}$  of our champion device is also higher than those of many highly efficient Sb<sub>2</sub>Se<sub>3</sub> devices in literature [5,26,30,31]. Given that the Sb<sub>2</sub>Se<sub>3</sub> grain size of 420-Sb<sub>2</sub>Se<sub>3</sub> device is comparable to that of Sb<sub>2</sub>Se<sub>3</sub> solar cells with top efficiencies [13,32], the remarkable  $V_{OC}$  of our Sb<sub>2</sub>Se<sub>3</sub> solar cell could be accounted for by optimized heterojunction quality, large built-in voltage and grain size that originated from the post selenization process.

#### 6. Defect characterization of devices

Defect activation energies and density of defects for the devices were investigated by admittance spectroscopy measured in the temperature range of 210–300 K. The temperature-dependent capacitancefrequency (*C*-*f*-*T*) spectra of the devices are shown in Fig. 6a. Larger capacitance variation with the decrease of temperature can be observed for the 380-Sb<sub>2</sub>Se<sub>3</sub> device, indicating higher defect density for the device since the capacitance reduction is directly related to dielectric freeze-out of defects at lower temperatures [33]. The inflection point for each admittance spectrum is determined by the Arrhenius plot and the inflection point frequency  $\omega_0$  of each curve is derived from the angular frequency point  $\omega$  at the maximum of the  $\omega dC/d\omega$  plot. The Arrhenius plot is linearly fitted based on the equation [34]:

$$\omega_0 = 2\pi v_0 T^2 \exp(\frac{-E_a}{kT}) \tag{3}$$

where  $\nu_0$  is the attempt-to-escape frequency,  $\omega_0$  is the inflection point frequency and  $E_a$  is the defect activation energy that represents the average energetic depth of the defect relative to the VBM or CBM [34]. The  $E_a$  values derived from the Arrhenius plots are 456 meV and 495 meV for the 420-Sb<sub>2</sub>Se<sub>3</sub> and 380-Sb<sub>2</sub>Se<sub>3</sub> device, respectively, as shown in Fig. 6b. As mentioned before, EDS results have revealed that all the Sb<sub>2</sub>Se<sub>3</sub> thin films prepared in this work are Se deficit apart from the 460-Sb<sub>2</sub>Se<sub>3</sub> device (Table 1). It is known that donor defects namely, antimony antisite  $Sb_{se}$  and selenium vacancy  $V_{se}$  are prone to form under Se deficit condition [35]. Since the defect activation energies of our devices are in good agreement with the theoretical results by firstprinciple calculation [35], the activation energies of 456 meV and 495 meV can be ascribed to  $V_{se}$  and  $Sb_{se}$ , respectively. Considering the difference between the two calculated defect activation energies for both devices is relatively small ( $\Delta E_a = 39 \text{ meV}$ ), it would be difficult to distinguish them from each other in the devices. What's more, given that  $E_a$  represents the average value of the defect activation energies within the devices, in practical situation, it is logical to believe that both kinds of defect would be present in devices. Therefore, in our case, we tentatively attribute  $V_{se}$  and  $Sb_{se}$  to the dominant defect of 420-Sb<sub>2</sub>Se<sub>3</sub> and 380-Sb<sub>2</sub>Se<sub>3</sub> device, respectively, as the activation energy of  $Sb_{se}$  is estimated to be 30 meV higher than that of  $V_{se}$ , according to the first-principle calculation [35]. Since defects with higher activation energy are more likely to behave as recombination centers [33], the 380-Sb<sub>2</sub>Se<sub>3</sub> device is expected to suffer from larger recombination center population and thus more severe decline of device performance.

The defect density of each device was Gaussian fitted using the Kimerling model [34] based on the following equation:

$$N_t(E(\omega)) = -\frac{V_d}{q\omega} \frac{dC}{d\omega} \cdot \frac{\omega}{kT}$$
(4)

where *E* is the energetic distance between the defect energy level and the VBM or CBM,  $V_d$  is the built-in voltage of the heterojunction,  $\omega$  is the angular frequency. The defect density spectra of 420-Sb<sub>2</sub>Se<sub>3</sub> and

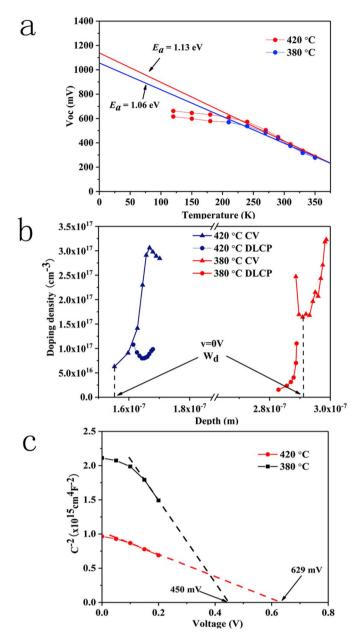
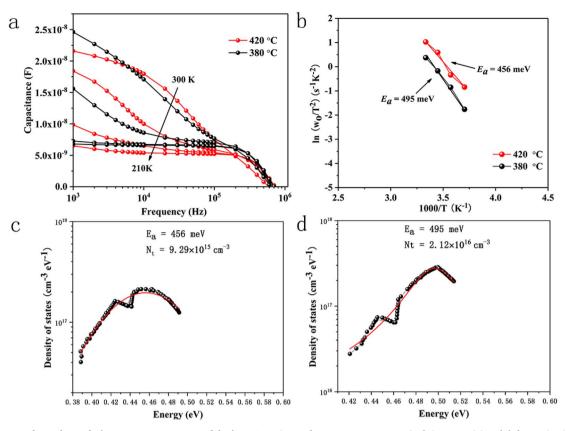


Fig. 5. Sb<sub>2</sub>Se<sub>3</sub>/CdS interfacial defect characterization of devices. Temperature-dependent open circuit voltage measurements (a), *CV* and *DLCP* profiling (b), and  $C^{-2}$ – *V* curves (c) of 380-Sb<sub>2</sub>Se<sub>3</sub> and 420-Sb<sub>2</sub>Se<sub>3</sub> devices.

380-Sb<sub>2</sub>Se<sub>3</sub> device are plotted in Fig. 6c and d, respectively, and not surprisingly, a larger defect density was obtained for the 380-Sb<sub>2</sub>Se<sub>3</sub> device. Based on the above results, we can conclude that the 380-Sb<sub>2</sub>Se<sub>3</sub> device possessed a higher population of donor defects, most of which are *Sb<sub>se</sub>* antisites with deeper energy levels than *V<sub>se</sub>*. A large number of deep defects will act as recombination centers, yielding recombination losses both in the Sb<sub>2</sub>Se<sub>3</sub> layer and the heterojunction interface which can significantly degrade the conversion efficiency of the 380-Sb<sub>2</sub>Se<sub>3</sub> device. On the other hand, annealing the Sb<sub>2</sub>Se<sub>3</sub> thin films under an optimized selenization temperature (420 °C) can effectively passivate deep defects for the device by making the films towards stoichiometric composition. Of course, the contribution of the reduced recombination rate induced by less defects that originated from the proper crystal orientation and crystallinity should not be ruled out as well.



**Fig. 6. Temperature-dependent admittance measurements of devices.** Capacitance-frequency-temperature (*C-f-T*) spectra (**a**) and defect activation energies (**b**) of the two devices. Defect density spectra of 420-Sb<sub>2</sub>Se<sub>3</sub> device (**c**) and 380-Sb<sub>2</sub>Se<sub>3</sub> device (**d**) derived from admittance spectra.

#### 7. Conclusions

In summary, we have demonstrated the fabrication of highly efficient and stable  $Sb_2Se_3$  thin film solar cells by magnetron sputtering. A post selenization process was introduced in this work to optimize the  $Sb_2Se_3$  absorber layer in terms of crystallinity, crystal orientation, chemical composition and grain size etc. Selenization temperature is found to be crucial for the  $Sb_2Se_3$  thin film quality. Charge carrier transport optimization, heterojunction interface adhesion improvement as well as defect passivation both in the film and at the interface can be effectively achieved by selecting the proper selenization temperature. After carefully optimizing the selenization process, a final device with a conversion efficiency of 6.06% has been obtained, which represents the highest PCE of sputtered  $Sb_2Se_3$  planar heterojunction solar cells.

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#### Appendix A. Supplementary data

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