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# Mechanical and Thermomechanical Characterization of Different Leathers

Noëlie Di Cesare, Guillaume Corvec, Xavier Balandraud, Jean-Benoît Le Cam, and Julien Gauffreteau

**Abstract** Leather materials are able to undergo various strain and stress states during their elaboration process and their use in numerous applications. Although the experimental mechanical response in tension of leathers has been studied in the literature for decades, scarce information is available on the nature of their elasticity and more generally on their thermomechanical behaviors. In the present study, two leathers were tested under uniaxial cyclic loading while temperature changes were measured at the specimens' surface by infrared thermography. The heat power at the origin of the temperature changes was then determined by using an adequate version of heat diffusion equation which is applicable to homogeneous tests. Results enabled us to discuss on the physical nature of the thermoelastic coupling in leathers. Intrinsic dissipation caused by the mechanical irreversibility was also detected. Distinct behaviors are evidenced as a function of the type of leathers.

**Keywords** Infrared thermography · Leather · Heat source · Thermoelastic coupling · Mechanical dissipation

## 12.1 Introduction

Although the experimental mechanical response in tension of leathers has been studied in the literature for decades [1–5], scarce information is available on the nature of their elasticity and more generally on their thermomechanical behaviors. Some physical phenomena involved in their deformation mechanism have been proposed to model their mechanical response in terms of stiffness, rupture or relaxation. Beyond mechanical tests, some measurements carried out by using infrared (IR) thermography have been performed to analyze the temperature variations at the surface of leathers. Two types of approach are reported in the literature:

- application to non-destructive control of final leather products [6]. In this case, pulsed-phase thermography was performed to evidence hidden scratches and the texture in depth, and finally to evaluate the quality of the leather;
- analysis of the thermal response of leathers under mechanical loading [7–9]. More precisely, applications concerned the self-heating under cyclic loading, with the main objective of determining a limit of acceptable damage for leather products.

The present study belongs to the second type of approach and aims at studying the thermomechanical response of leathers under cyclic mechanical loading, more precisely under load-unload cycles. Due to thermomechanical couplings, any material produces or absorbs heat when stretched. In particular, thermoelastic couplings occur in any material. Two types of thermoelastic couplings can be distinguished: a “classical” thermoelastic coupling, which is sometimes named *isentropic coupling* [10] and occurs in metallic materials and polymers below their glass transition temperature; an *entropic coupling*, which occurs in rubber-like materials [11]. Rubber-like materials actually feature both types of thermoelastic coupling. Even though the entropic coupling is preponderant, the thermoelastic coupling occurs and is response for the

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N. Di Cesare  
Université Bretagne Sud, IUT de Lorient-Pontivy, IRDL, FRE CNRS 3744, Pontivy, France

G. Corvec · J.-B. Le Cam (✉)  
Univ Rennes, CNRS, IPR (Institute de Physique de Rennes) – UMR 6251, Rennes, France

LC-DRIME, Joint Research Laboratory, Cooper Standard – Institut de Physique UMR 6251, Rennes Cedex, France  
e-mail: jean-benoit.lecam@univ-rennes1.fr

X. Balandraud  
Université Clermont Auvergne, CNRS, SIGMA Clermont, Institut Pascal, Clermont-Ferrand, France

J. Gauffreteau  
SIGMA Clermont, Campus Design, Matériaux & Innovation, Aubière Cedex, France

*thermoelastic inversion* at low strains [12, 13]. Any mechanical irreversibility occurring in a material is also accompanied by heat production: plasticity, fatigue damage and viscosity are all associated with a heat production leading to material self-heating, i.e. a global increase in temperature. Measuring temperature changes at the surface of tested specimens is thus relevant to improve our understanding of materials' behavior. However, the analysis of the heat sources provides more relevant information than the analysis of the temperature changes (By "heat source", we mean the heat power density in  $\text{W/m}^3$  produced or absorbed by the material itself due to a change in the mechanical state). Indeed, temperature is affected by the heat diffusion in the specimen and with the outside of the specimen (by conduction with the jaws of the testing machine, by convection with ambient air) and by radiations. Therefore, heat source is a "more intrinsic" quantity for investigating damage and deformation mechanisms. The heat source fields are reconstructed from the temperature fields and the heat diffusion equation [14, 15]. A zero-dimensional (0D) version of this equation can be employed when heat sources are homogeneous in the specimen, typically when the strain fields are homogeneous. This approach was used for rubbers [16–22], shape-memory alloys [23–29], polyamide 6.6 [30–34], PMMA [35], aluminum alloy [36], steel [37], copper [35, 38]. To the best knowledge of the authors, heat source calculation has never been performed in case of leathers.

In the present study, two leathers were tested under uniaxial cyclic loading while temperature changes were measured at the specimens' surface by using IR thermography. The heat power density at the origin of the temperature changes was then determined using the 0D version of the heat diffusion equation to analyze the thermomechanical response of the tested leathers.

## 12.2 Experimental Set-Up

The experimental set-up is presented in Fig. 12.1. Tests were conducted with a uniaxial testing machine featuring two actuators. Specimens were cut in a split cow leather (L1) and a grain calf leather (L2). A sample made of the same material as that tested was also used as a reference in order to follow the variation in the close environment. It was therefore not stretched. The free length of both specimens was equal to 63 mm. Tests were performed at ambient temperature. The loading consisted of load-unload cycles at a displacement rate of  $\pm 100$  mm/min. Two blocks of 6 cycles were successively applied. The maximum stretch was set to a quarter and a half of the stretch at failure for the first and second block, respectively.

Temperature measurements were performed by using a FLIR infrared camera equipped with a focal plane array of  $640 \times 512$  pixels and detectors operating in wavelengths between 1.5 and 5.1  $\mu\text{m}$ . The integration time was equal to 1000  $\mu\text{s}$  and the acquisition frequency was the same as for kinematic images, i.e. 25 fps. The thermal resolution or noise equivalent temperature difference is equal to 20 mK for a temperature range between 5 and 40  $^\circ\text{C}$ . The infrared camera was switched

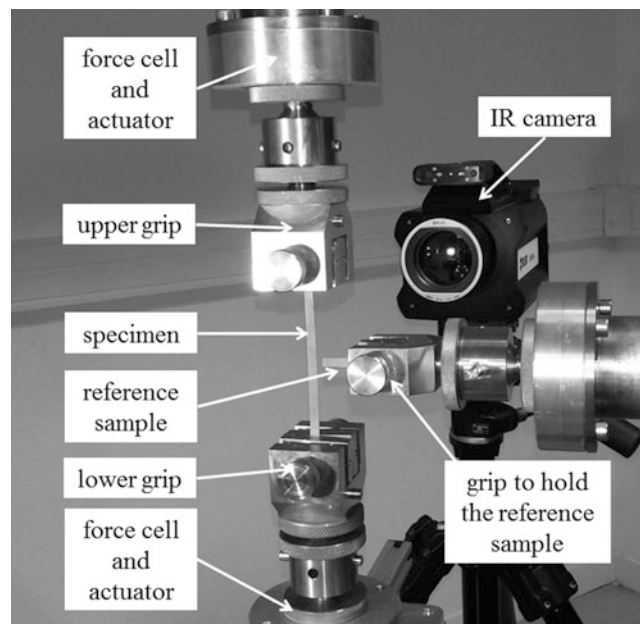


Fig. 12.1 Experimental configuration

on at least 3 h before testing in order to ensure its internal temperature to be stabilized. The calibration of camera detectors was performed with a black body using a Non-Uniformity Correction (NUC) procedure. The variation in mean temperature change of the tested specimen was defined with respect to the reference sample. A spatial averaging over the central zone of the specimen enabled us to improve the thermal measurement resolution.

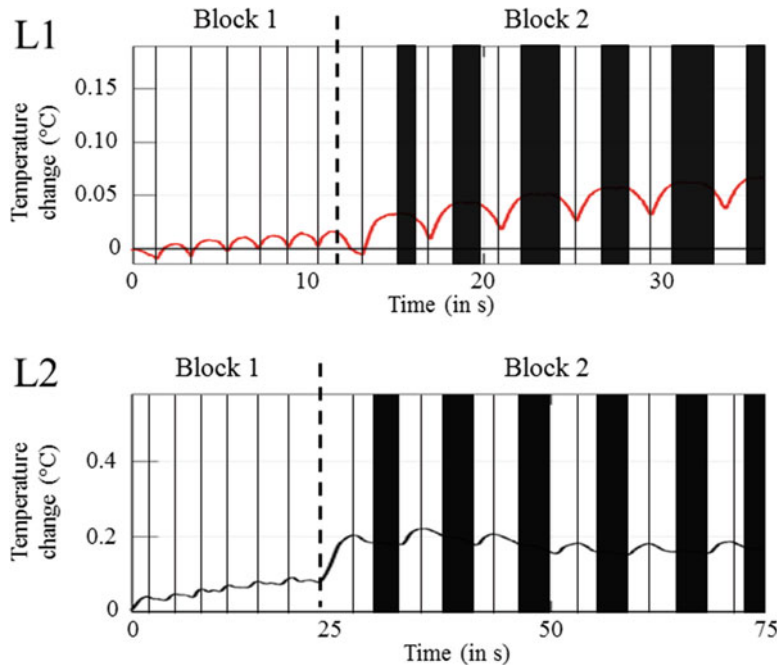
Tests were conducted with a home-made biaxial testing machine. Four independent RCP4-RA6C-I-56P-4-300-P3-M (IAI) electrical actuators enabled us to stretch symmetrically the samples. They were driven by a PCON CA 56P I PLP 2 0 controller and four PCON-CA (IAI) controller position coupled to a homemade LabView program. The cell load capacity was 1094 N. In the present case, the testing machine was used to stretch the precut sample with two actuators, i.e. with a neutral point in the specimen's middle, which enabled us to avoid complex displacement compensation processing.

### 12.3 Results

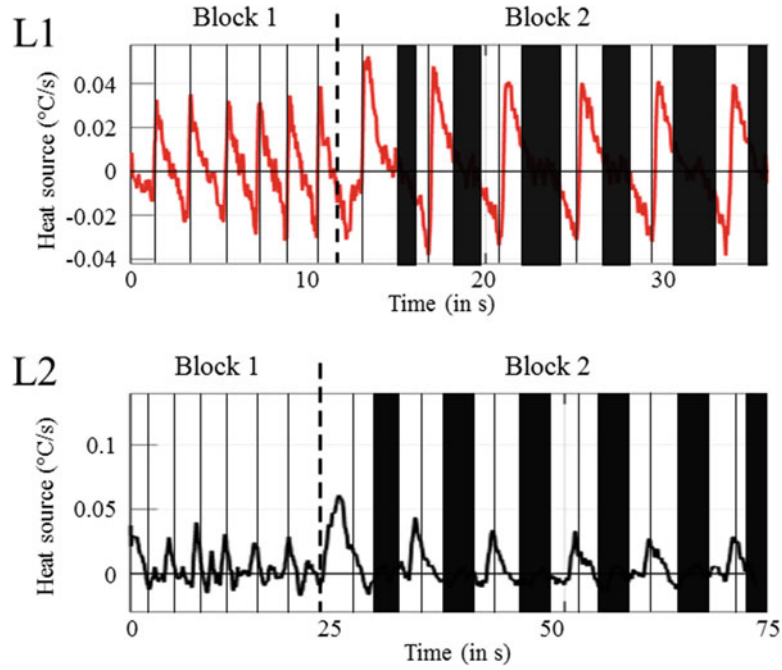
Figure 12.2 shows the mean temperature change as a function of time for both specimens. In both cases, buckling occurred upon unloading in the second block of cycles. Zones corresponding to buckling are highlighted by black rectangles in the graphs. The times corresponding to maximum stretching are indicated by vertical solid lines. Distinct responses are clearly observed. For material L1, temperature was decreasing during the loading phases, and was increasing during the unloading phases. This response is typical of materials featuring an *isentropic coupling*. An opposite behavior is observed for material L2, which thus features an *entropic coupling*. Mechanical dissipation can also be detected from these curves. Indeed for both materials, temperatures was globally increasing over the cycles (*positive* temperature changes), meaning that the total heat produced by the material over the cycles was positive. In other words, the heat produced is higher that the heat absorbed over one mechanical cycle. The next paragraph provides an analysis in terms of heat source variation.

As indicated in the introduction section, the 0D approach was applied to calculate the heat sources in relation to the measured temperatures. Equation (12.1) provides the relation between the heat source  $s$  (in  $W/m^3$ ) and the mean temperature change  $\theta$ :

$$s = \rho C \left( \frac{d\theta}{dt} + \frac{\theta}{\tau} \right) \quad (12.1)$$



**Fig. 12.2** Mean temperature change as a function of time for both specimens. Periods for which specimen buckling occurred are highlighted by black rectangles. The times corresponding to maximum stretching are indicated by vertical solid lines



**Fig. 12.3** Heat sources as a function of time for both specimens. Periods for which specimen buckling occurred are highlighted by black rectangles. The times corresponding to maximum stretching are indicated by vertical solid lines

where  $\rho$  is the material density,  $C$  the specific heat and  $\tau$  a time constant characterizing the global heat exchanges with the outside of the specimen. The value of  $\tau$  was preliminary measured for each specimen by considering a natural return to ambient temperature. By dividing Eq. (12.1) by  $\rho C$ , it comes

$$s' = \frac{d\theta}{dt} + \frac{\theta}{\tau} \quad (12.2)$$

where

$$s' = \frac{s}{\rho C} \quad (12.3)$$

which can be still named “heat source”, but then expressed in  $^{\circ}\text{C}/\text{s}$ . It corresponds to the temperature rate that would be obtained in adiabatic conditions. Figure 12.3 shows the heat source as a function of time for both specimens. For material L1, heat sources are positive during the loading phases, and negative during the unloading phases, due to an *isentropic coupling*. Opposite signs are observed for material L2, as expected for an *entropic coupling*. By temporal integration over each cycle, it can be shown that the total produced heat is positive. As the heat due to the thermoelastic couplings is null over a cycle, it means that both materials produced mechanical dissipation.

## 12.4 Conclusion

Two leathers were tested under uniaxial cyclic loading while temperature changes were measured at the specimens’ surface by using IR thermography. By calculating the heat sources at the origin of the temperature changes, the nature of the thermoelastic coupling was identified. Intrinsic dissipation caused by the mechanical irreversibility was also detected. This type of results could be used to propose accurate thermomechanical behavior laws of leathers.

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