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Impact of the post-thermal annealing on OFETs using printed contacts, printed organic gate insulator and evaporated C₆₀ active layer

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Abstract

Towards fully printed organic electronics, bottom-gate, bottom contacts fullerene based organic FETs (OFETs) are fabricated using inkjet printing drop-on-demand technology for the deposition of gate contact, organic gate insulator and source and drain contacts. The last layer of this structure that is the semiconducting fullerene C₆₀ film, is deposited by thermal evaporation at ambient temperature. Using physical and electrical analysis, the electrical performances are optimized by studying the effect of the thickness of the C₆₀ film and of the post-thermal annealing of the OFET. A quantitative relationship between the crystalline structure of the C₆₀ semiconducting layer (grain size and surface roughness) and the electrical performance of the OFETs is demonstrated. The best performance as determined from the values of the electrical parameters of the OFETs are obtained for 90 nm thick C₆₀ film and after an annealing of the OFET at 200°C. The answer of present nearly fully printed OFETs to a voltage pulse applied to the gate lead to a switching time of 13 ms, and then to application frequency of some 10Hz. This result opens the way to potential main application in electronic circuits for the treatment of analog signals coming from the human body activities.

Keywords: inkjet printing drop-on-demand, Organic FET, physical characterization, electrical characterization, post-thermal annealing, time answer

1 Introduction:

Now, flexible electronics becomes a major research domain due to the fast-growing market. The overall revenue of wearable technology was \$38 billion in 2017 and it is expected to grow over \$85 billion in 2022 [1]. The dominant sectors will be the healthcare and medical, fitness and wellness. The main requirement for flexible or even stretchable devices is the use of ultra-flexible materials. The first parameter indicating the flexibility of a material is its Young modulus. With their very low Young modulus, organic materials are considered fitting perfectly the requirement of flexibility. The main purpose is then to fabricate electronic devices using organic materials.

P-type Organic Field Effect Transistors (OFETs) have exhibited the better performance compared with n-type OFETs. However, for the most efficient electronics, both N-type and P-type OFETs are demanded. Then, intense research is done to increase the performance of N-type OFETs. Among n-type organic semiconductors, fullerene shows great potential with reliable common field effect mobility close to $1 \text{ cm}^2\text{V}^{-1}\text{s}^{-1}$ [2]. The field effect mobility has been even higher, $6 \text{ cm}^2\text{V}^{-1}\text{s}^{-1}$, by using fullerene deposited at 250°C by hot-wall epitaxy [3]. Fullerene OFET presents not only interesting mobility but also a high electrical stability. By changing the gate insulator, *Zhang et. al* [4] succeeded in fabricating fullerene based OFET with high electrical stability under continuous polarization. The drain current degradation was about 3.1% during 2 h under bias stress. These performances were obtained thanks to the use of photolithography process and high cost deposition techniques. Indeed, to fabricate organic transistors, technologies involve usual deposition and photolithography techniques [5] and other new ones as deposition in solution by different ways spin-coating, drop-casting and printing using shadow hard or software masks [6,7].

Considering the huge promising market, the chosen technology has to be made easily at the lowest cost possible, on large area and at enough low temperature to be compatible with flexible substrate. Deposition in solution, particularly printing technology, fulfill these requirements and become now more and more used. Among several printing technologies, inkjet printing drop-on-demand technology is more promising [8,9]. More than the common properties of these techniques, low cost and easy to use, inkjet printing adds the low consumption of materials, the well-controlled process leading to considerable reproducibility and the possibility to fabricate very small features.

Present work fits with the perspective of low cost and easy processed fully organic electronics, by trying to fabricate bottom-gate, bottom contacts fullerene based OFETS using inkjet printing drop-on-demand technology. Our previous works [10,11] optimized the printing of silver on glass as gate contact and on photoresist SU8 as source and drain contacts and the printing of this photoresist SU8 as gate insulator. The present work focuses on the deposition of fullerene C_{60} by thermal evaporation on the fully printed structure. Compared to evaporation technology

combined with photolithography processing, the solution process such as printing leads to thicker deposited films. Then, in a bottom-gate, bottom contacts structure of the OFETs, the high aspect ratio between the drain and source contacts and the gate insulator imposes the use of thick semiconducting active layer. Present work will highlight the influence of the thickness of the C_{60} active layer on the performance of nearly fully printed C_{60} based bottom gate – bottom contacts OFETs.

The effect of the post-thermal annealing on the as-fabricated OFETs with different thickness of C_{60} active layer will be studied also. In our knowledge, no such work, combining the studies of the thickness and the post-thermal annealing on C_{60} OFETs, was previously done. It will lead to determine the optimum OFET's processing parameters.

Consequently, for the first time, a quantitative relationship between the crystalline structure of the C_{60} active layer (grain size and surface roughness) and the electrical performance of the OFETs is demonstrated.

2 Experimental

2.1 Transistor fabrication and characterization

Fig.1 shows a schematic cross-section of the C_{60} OFET fabricated following bottom gate and bottom contacts geometry. This figure highlights the problematic of the high aspect ratio between the drain and source contacts and the gate insulator. The thickness of the active layer has to be enough to insure good coverage between the source and drain contacts.

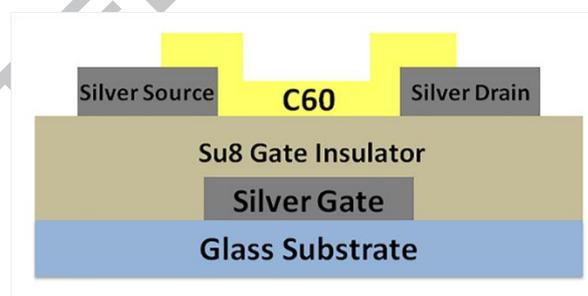


Fig. 1: Cross-section of the C_{60} OFETs using bottom gate and bottom contacts geometry. The figure highlights the problematic of the high aspect ratio between the drain and source contacts and the gate insulator

As illustrated in Fig.2, after cleaning the glass substrate with acetone, ethanol, and deionized water for 10 mins sequentially, the silver gate electrode was printed on the substrate (kepted at 50°C) with a thickness of 200nm using 256 nozzles Q-class printhead (Dimatix[®])(Fig2.b). Before spin coating the gate insulator layer, the substrate with silver gate electrodes is baked at 110°C for 30min allowing nanoparticles based ink sintering. Then, $1.2\mu\text{m}$ thick uncrosslinked SU8 2000 series photoresist (Bisphenol A Novolak epoxy; MicroChem) is spin-coated at a speed of 4500r/min during 60 seconds (Fig2.c). This layer will be used as polymeric gate insulator. After UV exposure and development (SU8 micro Dev, MicroChem), the SU8 layer was baked at 115°C during 15min. The baked SU8 layer is then submitted to 2mins

UV-Ozone treatment to adjust SU8 wetting behavior [10-12] ready for the printing of source and drain contacts. Drain and source electrodes were printed at 50°C using different patterns (width of the electrodes $W=4000\mu\text{m}$, distance between the electrodes $L=150\mu\text{m}$, and the thickness of the electrodes $D=205\text{nm}$ in Fig2.d). Finally, C_{60} film is thermally evaporated as the active layer of the transistor at room temperature under vacuum (2×10^{-7} mbar) with a constant deposition rate of 0.15A/s (Fig2.e).

The C_{60} active layer was deposited with four different thicknesses, 60 nm, 90 nm, 125nm and 250 nm in the purpose to study the effect of its thickness. The OFET is then characterized electrically, as deposited and after annealing at 3 different temperatures, 160°C, 200°C and 250°C, during 5 mins. Electrical characterization was performed in dark and under nitrogen atmosphere using a 2636A Keithley (Fig2.f).

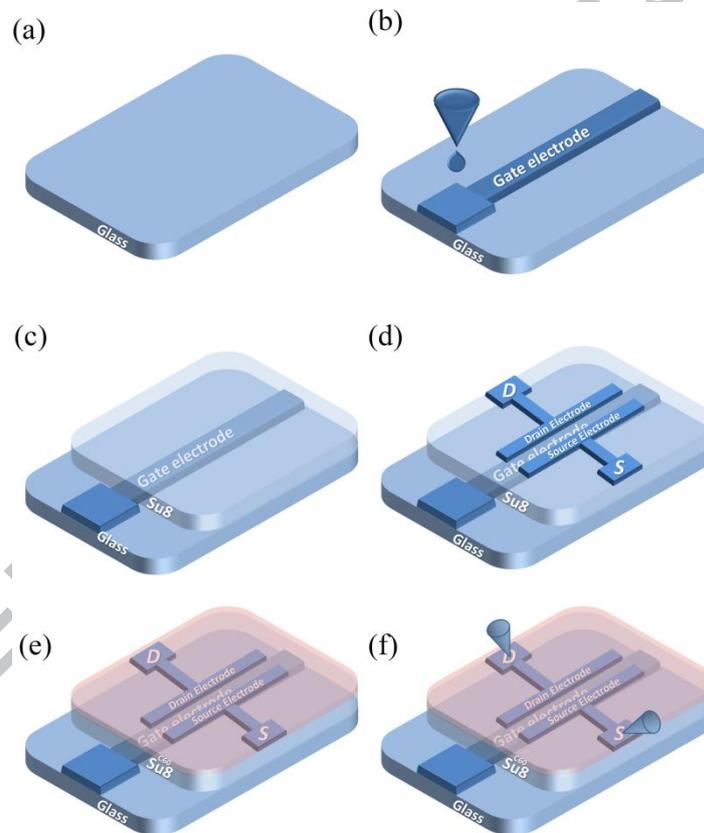


Fig. 2: Fabrication process of C_{60} OFET

2.2 Morphological characterization and topography parameters extraction of the C_{60} active layer.

In the purpose to study the effect of the temperature during the final annealing of the OFET, the morphology of the C_{60} active layer was analyzed using Atomic Force Microscopy (AFM). An Atomic Force Microscope (AFM VEECO Di Caliber) was utilized in tapping mode on an area of $1 \times 1 \mu\text{m}^2$. To describe the topography of the surface, we use the Power Spectral Density Function (PSDF). Its formulation is given by [26]:

$$S(f_x, f_y) = \frac{1}{L^2} \left| \sum_{m=1}^N \sum_{n=1}^N h_{nm} e^{2\pi i \Delta L (f_x n + f_y m)} (\Delta L)^2 \right|^2 \quad (1)$$

Here S is the 2-dimensional PSDF, L^2 is the scanned surface area, N is the number of data points in both X and Y direction of scanned area, h_{nm} is the surface profile height at position (m,n), f_x and f_y are the spatial frequencies in X and Y directions respectively, ΔL is the sampling interval. Based on the AFM images ($1\mu\text{m} \times 1\mu\text{m}$), the RMS roughness (σ) and the lateral correlation length (τ) were calculated from these PSDF functions (support files). Besides, the lateral correlation length (τ) is related to the grain size.

2.3 Electrical parameter extraction

As the most important electrical parameters, the field effect mobility μ ($\text{cm}^2 \cdot \text{V} \cdot \text{s}^{-1}$), the sub-threshold slope SS ($\text{V} \cdot \text{decade}^{-1}$), the threshold voltage V_{TH} (V), the contact resistance R_c (Ω), the minimum off-state current I_{off} (A), the on/off current ratio $I_{\text{on}}/I_{\text{off}}$ are utilized to evaluate the performance of the thin-film transistor.

In linear regime, μ , SS and V_{TH} are calculated from the equation 2 of the drain current I_D ($V_{\text{DS}} \ll (V_{\text{GS}} - V_{\text{TH}})$):

$$I_D = \frac{W}{L} \mu C_{\text{ins}} (V_{\text{GS}} - V_{\text{TH}}) V_{\text{DS}} \quad (2)$$

Where the W , L and C_{ins} are the width, the length of the channel and the capacitance of the gate insulator per area unit, respectively. The slope of I_D - V_{GS} curve at constant V_{DS} is the transconductance g_m given by:

$$g_m = \mu \frac{W C_{\text{ins}} V_{\text{DS}}}{L} \quad (3)$$

The threshold voltage V_{TH} is the gate voltage axis intercept of I_D - V_{GS} curve plotted in linear part. The field effect mobility μ is deduced from the extraction of g_m .

The subthreshold slope SS is extracted from I_D - V_{GS} curve plotted in semi-logarithmic scale using:

$$SS = \left(\frac{\partial \log I_D}{\partial V_{\text{GS}}} \right)_{\text{Max}}^{-1} \quad (4)$$

The contact resistance R_c is calculated from the equation of the drain-source resistance R_{DS} :

$$R_{\text{DS}} = \frac{V_{\text{DS}}}{I_D} = 2R_c + \left(\frac{L}{W \mu C_{\text{ins}}} \right) \frac{1}{V_{\text{G}} - V_{\text{TH}}} \quad (5)$$

where R_c is the contact resistance, assumed similar for both source and drain contacts.

3 Results and discussions

3.1 Effect of the semiconductor annealing temperature on the morphology of the C_{60} thin film on the OFET.

3.1.1 Morphology of C_{60} active layer as a function of the annealing temperature.

To study only the effect of the final annealing temperature of the OFET, on the

morphology of its C_{60} active layer, the thickness of this layer was fixed at 125nm. The morphology was studied as deposited and after annealing at 160°C, 200°C, 250°C. As illustrated in Fig.3, the 2D, 3D and line scan AFM images of C_{60} thin film as deposited and after annealing at 160°C, 200°C and 250°C exhibit that C_{60} morphology depends on the annealing temperature. From the 2D AFM images, the surface roughness increases and the number of grains decreases in the same area when the annealing temperature increases. Quantitatively, the RMS roughness s and grain size t were calculated using the equation (1) and reported in Table 1.

Table 1: RMS roughness and grain size calculated using PSDF formulation (1)

Annealing Temperature (°C)	Roughness σ (nm)	Grain size τ (nm)
As-deposited	1.42	4.72
160	1.75	7.70
200	1.91	13.46
250	2.72	14.16

Morphological parameters (roughness and grain sizes values) continuously increase when annealing temperatures increase. Furthermore, the grain size increases more when such temperature is below 200°C than between 200°C and 250°C.

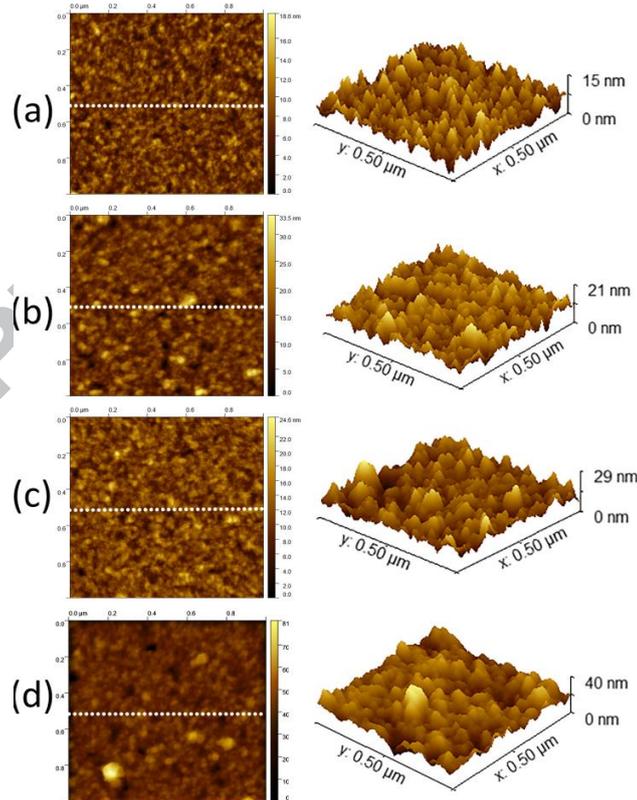


Fig. 3: 2D ($1 \times 1 \mu\text{m}^2$) AFM images, corresponding 3D enlarged ($0.5 \times 0.5 \mu\text{m}^2$) (a) as-deposited; and after annealing at 160°C (b), 200°C (c) and 250°C (d)

3.2.1 OFET with 125 nm thick C_{60} active layer as a function of the annealing temperature

Fig.4 shows the mean transfer and output characteristics of 4 OFETs as-fabricated

and after an annealing at 3 different temperatures, 160°C, 200°C and 250°C. All the OFETs have the same size (channel width and length equals to 4000 μm and 150 μm , respectively).

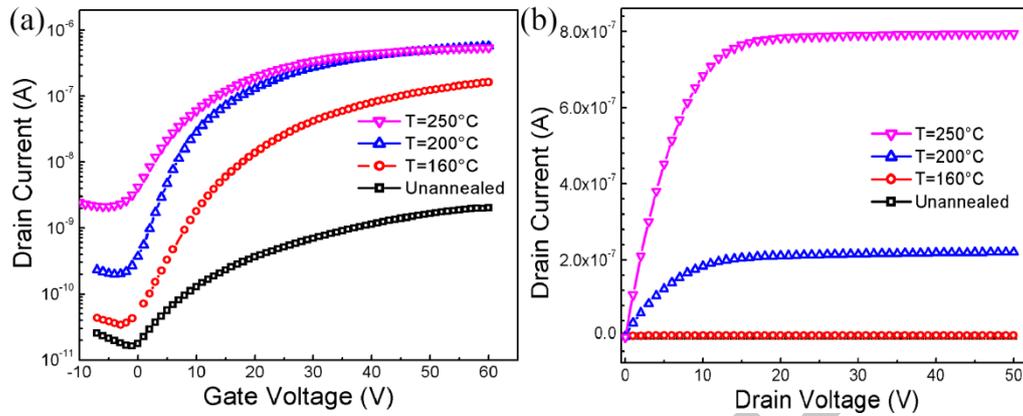


Fig.4: (a) Mean transfer characteristics ($V_D=20\text{V}$) and (b) output characteristics ($V_G=20\text{V}$) of several OFETs having the same size (channel width $W=4000\ \mu\text{m}$, channel length $L=150\ \mu\text{m}$) and 125 nm thick C_{60} active layer, measured as-fabricated and after annealing at 160°C, 200°C and 250°C.

All the OFET's parameters such as threshold voltage, subthreshold slope, field effect mobility, on-current, improve when the annealing temperature increases. The value of these parameters is reported in Table 2 and plotted as a function of the annealing temperature in Fig. 5a.

Table 2

Main mean electrical parameters of several OFETs having the same size (channel width $W=4000\ \mu\text{m}$, channel length $L=150\ \mu\text{m}$) and 125 nm thick C_{60} active layer, measured as-fabricated and after annealing at $T_A=160^\circ\text{C}$, 200°C and 250°C. V_{TH} is the threshold voltage, SS the subthreshold slope, μ the field effect mobility, R_C the contact resistance, μ after R_C the mobility after correction by R_C , I_{off} is the minimum current and I_{on}/I_{off} is the ratio between the maximum current and the minimum current

T_A (°C)	V_{TH} (V)	SS (V/dec)	μ ($\text{cm}^2/\text{V.s}$)	R_C (Ω)	μ after R_C ($\text{cm}^2/\text{V.s}$)	I_{off} (A)	I_{on}/I_{off}
Unannealed	19.3	9.3	5.3×10^{-5}	8×10^6	5.8×10^{-5}	1.6×10^{-11}	125
160	20	7	4.2×10^{-3}	2×10^6	4.47×10^{-3}	3.4×10^{-11}	4.7×10^3
200	11.2	4	1.44×10^{-2}	1.7×10^6	1.46×10^{-2}	2×10^{-10}	2.85×10^3
250	6.2	6.2	1.46×10^{-2}	2×10^6	1.5×10^{-2}	2×10^{-9}	270

Table 2 highlights that the main electrical parameters (i.e., threshold voltage, subthreshold slope, mobility) are strongly impacted by annealing temperature (especially below 200°C). It seems that these electrical parameters are governed by the grain size.

The contact resistance decreases after the annealing at 160°C and then stabilizes. Its value stays much lower than the channel resistance and then the corrected mobility by removing the effect of the contact resistance, does not change drastically. This conclusion was expected due to the starting linear increase of the drain current as can be observed in the output characteristics. Moreover, the off-current increases when the

annealing temperature increases. The increase seems to be due to the improvement of the active layer after annealing and then to better conductive layer. Considering these preliminary observations, it seems that the optimum annealing temperature is 200°C. The different parameters after this annealing are similar to the 250°C annealing ones. Moreover, the on-current to off-current ratio is higher than its value after 250°C annealing.

To understand the behavior of the main parameters depending on the annealing temperature, we can try to highlight a relationship between the AFM and the electrical characterizations. The mobility and the grain size present similar behavior as shown in Fig. 5b. Both, mobility and grain size strongly increase when temperature increases until 200°C and a little bit when the grain size increases between 200°C and 250°C. The subthreshold slope SS presents a specific behavior as it increases between 200°C and 250°C. Such behavior can be understood from the usual equation of SS (6) as a function of the defects density in the channel N_{ep} and at the interface between the channel and the gate insulator N_{SS} [14]

$$SS = \frac{kT \ln(10)}{q} \left(1 + \sqrt{\frac{q^2 \epsilon_0 \epsilon_{sc} N_{ep}}{C_{ins}}} + \frac{q^2 N_{SS}}{C_{ins}} \right) \quad (6)$$

C_{ins} is the capacitance per area unit of the gate insulator and ϵ_{sc} is the relative dielectric constant of the semiconducting active layer.

On the one hand, if the C_{60} active layer is considered as a polycrystalline material, N_{ep} is the defect density concentrated mainly in the grain boundaries. The defect density at the interface N_{SS} depends at least partially on the roughness of the interface between the channel and the active layer. Note that, the grain size was previously determined by AFM measurements. Meanwhile, Fig.5c compares the behavior of SS , the roughness and the grain size determined from AFM measurements. SS decreases whereas the grain size and the roughness increase before 200°C. It seems that this decrease of SS is governed mainly by the decrease of the defect density inside the channel due to the increase of the grain size. Between 200°C and 250°C, SS increases, the grain size increases only a little bit however the roughness increases strongly. In conclusion, as the grain size and then the defect density inside the channel saturates more or less, the increase of SS is mainly attributed to the increase of the roughness.

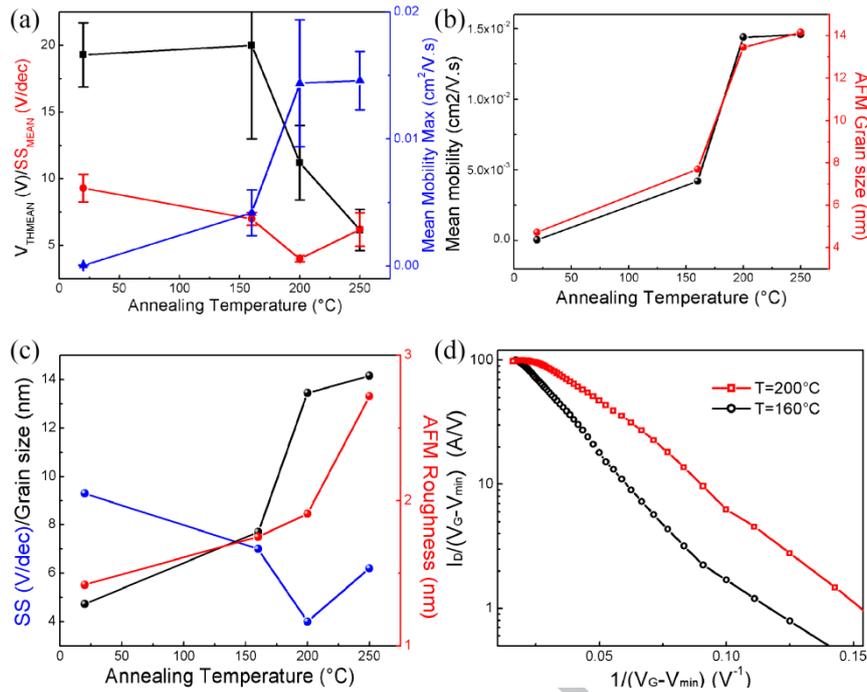


Fig.5: (a) Behavior of the mean threshold voltage V_{THMEAN} , subthreshold slope SS_{MEAN} and field effect mobility, when the annealing temperature increases; (b) Similar behavior of the mobility and the grain size as a function of the annealing temperature; (c) Behavior of the subthreshold slope SS , the surface roughness and the grain size as a function of the annealing temperature; (d) Semi-logarithmic plot of $I_D/(V_G-V_{min})$ versus $1/(V_G-V_{min})$ for OFETs annealed at 160°C and 200°C

Coming back to the link between the mobility and the grain size, the conduction models in polycrystalline materials can be apply, particularly the conduction in thin-film transistors with polycrystalline active layer. If we assume that polycrystalline materials are composed by a chain of crystalline regions with superficial discrete traps at the grain boundaries, the drain current, I_D , and the gate voltage, V_G , of these transistors are found [15-16] to be related in the subthreshold regime to:

$$(7)$$

W and L are the width and the length of the channel. C_{ins} is the capacitance per area unit of the gate insulator. V_{min} is the gate voltage at the minimum of I_D from which the channel start to form and then I_D start to increase. V_D is the drain voltage. q is the electronic charge. t is the thickness of the channel. N_T , is the superficial concentration of defects in the grain boundaries. ϵ_s is the permittivity of the semiconducting active layer. kT is the thermal energy.

In this model [17], the mobility is thermally activated following the relationship:

$$(8)$$

where E_b is the barrier energy at the grain boundary.

The relation (7) is valid when the electron concentration in the channel (in the case of N-type transistor) is larger than a critical concentration $N^*=N_T/G$ in which G is the size of the grains. Using this relation (7), the semi-logarithmic plot of $I_D/(V_G-V_{min})$ versus $1/(V_G-V_{min})$ may be fitted with a linear function. The slope of the

function is proportional to N_T^2 .

As shown in Fig.5d, semi-logarithmic plot for OFETs annealed at 160°C and 200°C. Both plots have a linear range. The departure from the linearity occurs at larger $1/(V_G - V_{min})$ and the slope of the linear functions is lower for 200°C annealed OFET than for 160°C annealed OFET, meaning lower slope for largest grain size OFET. Larger $1/(V_G - V_{min})$, corresponding then to larger $N^* = N_T/G$, means larger grains in 200°C annealed OFET.

The slope of the linear function can lead us to calculate N_T . Besides the physical constant q , ϵ_0 and k , the relative dielectric constants are taken 2.7 for SU8 gate insulator [18] and 5 for C_{60} film [19]. The thickness of the gate insulator is 1.2 μm . The actual unknown is the thickness t of the channel. To jump this difficulty, we can take the channel extending into the full thickness of the active layer that is not realistic, but can give an order of the minimum defect density in the grain boundaries. An order of the maximum defect density can be obtained considering very thin channel, 3 nm for example.

Taking then $t=125$ nm, the calculated superficial defect density N_T at the grain boundaries is $3 \times 10^{11}/\text{cm}^2$ and $2.5 \times 10^{11}/\text{cm}^2$ for 160°C and 200°C annealed OFETs. N_T increases to $1.9 \times 10^{12}/\text{cm}^2$ and $1.6 \times 10^{12}/\text{cm}^2$ for 160°C and 200°C annealed OFETs if we consider a channel thickness of 3 nm (~ 2 -unit cells of C_{60} crystalline network).

The first observation is the low defect density in the grain boundaries of such organic material. For comparison, the same model gives an order of $10^{12}/\text{cm}^2$ for N_T in polycrystalline silicon transistors considering a channel thickness of 30 nm [20].

The second observation is the slight difference between the values of N_T in both OFETs, even if N_T is lower in 200°C annealed OFETs. The large difference between the mobility values in these OFETs is mainly due to the large increase of the grain size and not to a decrease of the defect density inside the grain boundaries, leading to much lower $N^* = N_T/G$ ratio in 200°C annealed OFET. In conclusion, the mobility is primarily governed by the grain size (or the number of grains in the channel) than by the defect density in the grain boundaries. Importantly, this direct quantitative link between the physical structure of the active layer and the electrical parameters of organic transistor was never encountered in the literature in our knowledge.

In a summary of this section, the effect of the annealing temperature on printed C_{60} OFET's properties has been studied. Optimum parameters are obtained for 200°C annealing temperature. Furthermore, compare to OFET annealed at 250°C, OFET annealed at 200°C show similar mobility, lower subthreshold slope and higher on-current to off-current ratio.

3.3 Effect of the thickness of the C_{60} active layer on the OFET annealed at 200°C

Another experimental parameter that can influence the properties of the OFETs is the thickness of the C_{60} active layer. Following the previous study, the effect of this thickness on the properties of the OFETs, annealed at 200°C after their fabrication, is presented hereafter.

Fig. 6 shows the mean transfer and output characteristics of 4 OFETs having a C_{60} active layer with a thickness of 60nm, 90 nm, 125 nm or 250nm. All the OFETS have the same size, with a channel width $W=4000$ μm and a channel length $L=150$

μm . The best characteristics are obtained for an active layer of 90 nm thick. The behavior of the electrical parameters as a function of the thickness is shown also in Fig. 6c and their values are presented in Table 3. It seems that the low performance of the 60 nm thick active layer OFETs is probably due to low coverage between the active layer and the 205 nm thick source and drain contacts. The performance of 90 nm thick and 125 nm thick active layer OFETs are more or less similar with higher mobility for 90 nm thick OFET. The bad subthreshold slope of 250 nm thick active layer OFET can be mainly due to the high roughness of the surface.

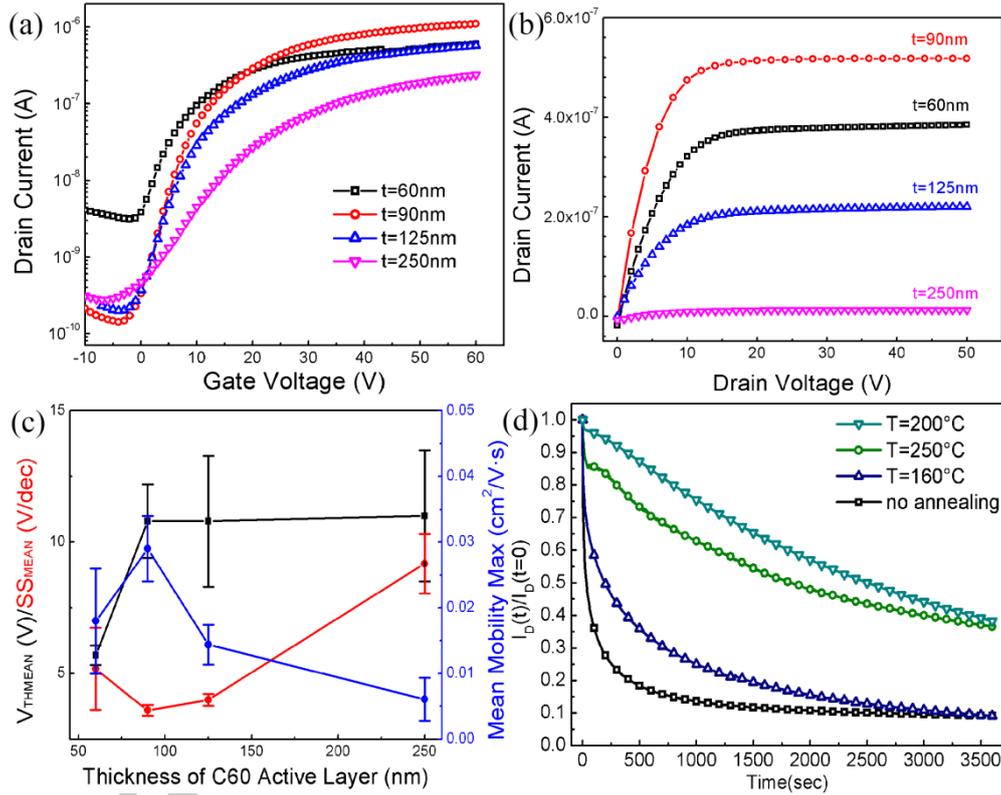


Fig. 6: (a), (b), (c): Mean transfer and output characteristics of several OFETs having the same size (channel width $W=4000 \mu\text{m}$, channel length $L=150 \mu\text{m}$) and a C_{60} active layer with a thickness of 60nm, 90 nm, 125 nm or 250nm. The behavior of their mean electrical parameters (Threshold voltage, subthreshold slope and mobility) is also reported. (d) Drain-current of OFETs using 90 nm thick C_{60} active layer un-annealed and annealed at different temperatures, 160°C, 200°C, 250°C as a function of the time under 40V gate-source voltage and 20V drain-source voltage

Table 3

Main mean electrical parameters of several OFETs having the same size (channel width $W=4000 \mu\text{m}$, channel length $L=150 \mu\text{m}$) and a C_{60} active layer with a thickness $t_{C_{60}}$ of 60nm, 90 nm, 125 nm or 250nm, all annealed at 200°C. V_{TH} is the threshold voltage, SS the subthreshold slope, μ the field effect mobility, R_c the contact resistance, μ after R_c the mobility after correction by R_c , I_{off} is the minimum current and I_{on}/I_{off} is the ratio between the maximum current and the minimum current.

$t_{C_{60}}$ (nm)	V_{TH} (V)	SS (V/dec)	μ ($\text{cm}^2/\text{V}\cdot\text{s}$)	R_c (Ω)	μ after R_c ($\text{cm}^2/\text{V}\cdot\text{s}$)	I_{off} (A)	I_{on}/I_{off}
60	5,7	5,2	1.8×10^{-2}	2.7×10^6	1.9×10^{-2}	3×10^{-9}	180

90	10,8	3,6	2.9×10^{-2}	7.5×10^5	2.95×10^{-2}	1.4×10^{-10}	7.8×10^3
125	10,8	4	1.4×10^{-2}	1.2×10^7	1.7×10^{-2}	2×10^{-10}	2.85×10^3
250	11	9,2	6.1×10^{-3}	1×10^7	6.5×10^{-3}	2.7×10^{-10}	870

In conclusion, the best conditions to prepare the evaporated C_{60} active layer of printed bottom-gate/bottom-contacts OFETs, are obtained with a thickness of 90 nm and a post-thermal annealing equal 200°C .

To re-inforce this conclusion, the drain-current of OFETs using 90 nm thick C_{60} active layer and annealed at different temperatures, was plotted as a function of the time when constant gate voltage V_{GS} and drain voltage V_{DS} are applied. Under $V_{GS}=40\text{V}$ and $V_{DS}=20\text{V}$, the drain current decreases with the time (Fig. 6d). In these conditions, the 200°C annealed OFETs have the slowest decrease leading to more reliable value of the current under constant biasing.

3.4 Dynamic behavior of the optimized printed C_{60} based OFET

Defining then the best conditions to prepare the evaporated C_{60} active layer of printed bottom-gate/bottom-contacts OFETs and knowing their static performances, is a prerequisite step to evaluate their optimum dynamic performance. The dynamic performance is studied through the behavior of resistive loaded OFET under square pulsed voltage applied to its gate.

Static output characteristic of the OFET as an inverter is presented in Fig.7. The load resistance R is fixed to $500\text{M}\Omega$ and the circuit is biased by $V_{DD}=20\text{V}$.

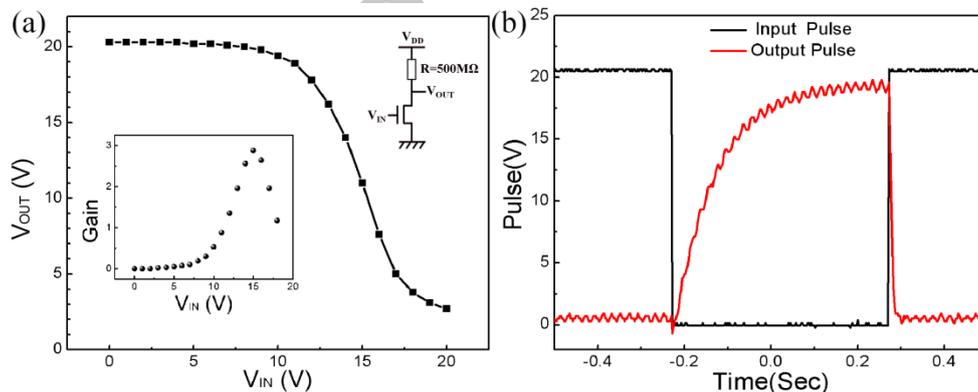


Fig. 7: (a) Static output characteristic of printed C_{60} based OFET loaded by $500\text{M}\Omega$ resistance and (b) its response to 1Hz pulse. The inset shows the gain of the inverter with a maximum value of 3.

In these polarization conditions, the inverter has a gain (maximum of the differentiation dV_{OUT}/dV_{IN}) of 3 (Fig.7a). This value depends on the load resistance of course. But, it is in the order of the gain of organic based OFETs inverters [21]. The minimum output voltage V_{OL} with the maximum input voltage V_{IN} is explained by the resistance value of the channel in on-state compared to the load resistance.

More interestingly than the static characteristic, the dynamic response of the OFET to a voltage pulse gives a better idea of its performance. When applying 20V pulse of 0.5 second duration (1 Hz frequency) to the gate of the OFET, the behavior of the output voltage gives its time response (as shown in fig.7b). When the gate-source voltage switches from 20V to 0V, the OFET status switches from the on-state to the off-state and then the output voltage has to switch from nearly 0V to nearly 20V. The

switch time is defined usually by the time from 10% to 90% of the maximum voltage. In the case of the present OFET, the switching time is 220 ms. This time is due to the load resistance as its value is much lower than the resistance of the channel in off-regime, 500M Ω compared to some hundreds G Ω .

The more significant time is the switching time between the off-state and the on-state that depends nearly only on the transistor. This time corresponds to the decrease of the output voltage from the maximum to the minimum value. The switching time from 90% to 10% of the maximum voltage is 13 ms here. Present OFET can answer to more than 10Hz frequency. However, the frequency can be increased more by optimizing the overlap between the gate contacts and source and drain contacts and by chemically modifying the surface of drain and source electrodes before the deposition of C₆₀ active layer as we have done previously for photolithography processed C₆₀ OFETs where 1.5 cm²/V.s was obtained [22]. In fact, the frequency can be considered depending on the applications. For example, 100Hz frequency is enough if OFETs are integrated into a treatment electronic circuit of signals coming from human body activities. Such 100Hz frequency can be reached with such process improvement.

4 Conclusion

The main purpose of present work was devoted to the optimization of the last deposited layer in bottom-gate bottom contacts printed C₆₀ based OFET. This last deposited layer is a film of C₆₀. The first steps of the process were the printing of the silver gate contact, the photoresist SU8 gate insulator, the drain and source silver contacts. All these steps were previously optimized and the results were published in different papers [10,11]

The effect of the post-annealing temperature of the fabricated OFET was studied firstly. Direct correlation between the structure of the C₆₀ film (grain size, surface roughness) as analyzed from AFM observation and electrical parameters of the OFET was highlighted. More than the correlation, proportionality between the grain size and the field effect mobility was evidenced. The surface roughness is effective only when the grain size does not change a lot. The proportionality between the grain size and the mobility led us to involve the usual Seto model [17] and its derivatives established for polycrystalline films and thin film transistors based on. Treatment of the experimental curves fit well with this model leading us to the calculation of the defect density in the grain boundaries. In our knowledge, such detailed analysis was never made before on the effect of the post-annealing temperature on organic transistors. Determining the 200°C optimum post-annealing temperature, the thickness of the C₆₀ active layer was optimized at 90 nm and confirmed by electrical stability study of the drain current during continuous polarization of the transistor. Considering the potential main application of such transistors in electronic circuits for the treatment of analog signals coming from the human body activities, the response of present OFETs to a voltage pulse applied to the gate was measured. A switching time of 13 ms was obtained, leading to application frequency of some 10Hz.

Future work on the optimization of the overlap between the contacts and on the

chemical modification of the surface of the contacts will be done soon in the goal to improve the stability and to increase the working frequency. The use of active charge (another NMOS OFET) in pseudo-CMOS inverter will be integrated soon in the purpose to get symmetric answer to a voltage pulse (similar rise time and fall time) will be done very soon. Finally, the integration of printed pentacene based P-type OFET is planned to reach the final goal of CMOS electronics.

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Figure Captions

Fig. 1: Cross-section of the C₆₀ OFETs using bottom gate and bottom contacts geometry. The figure highlights the problematic of the high aspect ratio between the drain and source contacts and the gate insulator

Fig. 2: Fabrication process of C₆₀ OFET

Fig. 3: 2D ($1 \times 1 \mu\text{m}^2$) AFM images, corresponding 3D enlarged ($0.5 \times 0.5 \mu\text{m}^2$) (a) as-deposited; and after annealing at 160°C (b), 200°C (c) and 250°C (d)

Fig. 4: (a) Mean transfer characteristics ($V_D=20\text{V}$) and (b) output characteristics ($V_G=20\text{V}$) of several OFETs having the same size (channel width $W=4000 \mu\text{m}$, channel length $L=150 \mu\text{m}$) and 125 nm thick C₆₀ active layer, measured as-fabricated and after annealing at 160°C, 200°C and 250°C.

Fig. 5: (a) Behavior of the mean threshold voltage V_{THMEAN} , subthreshold slope SS_{MEAN} and field effect mobility, when the annealing temperature increases; (b) Similar behavior of the mobility and the grain size as a function of the annealing temperature; (c) Behavior of the subthreshold slope SS , the surface roughness and the grain size as a function of the annealing temperature; (d) Semi-logarithmic plot of $I_D/(V_G-V_{\text{min}})$ versus $1/(V_G-V_{\text{min}})$ for OFETs annealed at 160°C and 200°C

Fig. 6: (a), (b), (c): Mean transfer and output characteristics of several OFETs having the same size (channel width $W=4000 \mu\text{m}$, channel length $L=150 \mu\text{m}$) and a C₆₀ active layer with a thickness of 60nm, 90 nm, 125 nm or 250nm. The behavior of their mean electrical parameters (Threshold voltage, subthreshold slope and mobility) is also reported. (d) Drain-current of OFETs using 90 nm thick C₆₀ active layer un-annealed and annealed at different temperatures, 160°C, 200°C, 250°C as a function of the time under 40V gate-source voltage and 20V drain-source voltage

Fig. 7: (a) Static output characteristic of printed C₆₀ based OFET loaded by 500M Ω resistance and (b) its response to 1Hz pulse. The inset shows the gain of the inverter with a maximum value of 3.

Table Captions

Table 1: RMS roughness and grain size calculated using PSDF formulation (1)

Table 2: Main mean electrical parameters of several OFETs having the same size (channel width $W=4000 \mu\text{m}$, channel length $L=150 \mu\text{m}$) and 125 nm thick C₆₀ active layer, measured as-fabricated and after annealing at $T_A=160^\circ\text{C}$, 200°C and 250°C. V_{TH} is the threshold voltage, SS the subthreshold slope, μ the field effect mobility, R_C the contact resistance, μ after R_C the mobility after correction by R_C , I_{off} is the minimum current and $I_{\text{on}}/I_{\text{off}}$ is the ratio between the maximum current and the minimum current

Table 3: Main mean electrical parameters of several OFETs having the same size (channel width $W=4000 \mu\text{m}$, channel length $L=150 \mu\text{m}$) and a C₆₀ active layer with a thickness t_{C60} of 60nm, 90 nm, 125 nm or 250nm, all annealed at 200°C. V_{TH} is the threshold voltage, SS the subthreshold slope, μ the field effect mobility, R_C the contact resistance, μ after R_C the mobility after correction by R_C , I_{off} is the minimum current and $I_{\text{on}}/I_{\text{off}}$ is the ratio between the maximum current and the minimum current.

- Investigation of thermal annealing process influence on printed n-type OFET
- Investigation of organic semiconductor layer thickness impacts on C₆₀ OFET
- Investigation on relationships between OFET stability and C₆₀ crystalline structure
- Investigation on Pseudo-CMOS inverter logic circuits

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