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# Microstructure and Mechanical Properties of a-CN<sub>x</sub> Films Prepared by Bias Voltage Assisted PLD with Carbon Nitride Target

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**Abstract:** Amorphous carbon nitride (a-CN<sub>x</sub>) films were deposited on silicon substrates using pulsed laser deposition technique (PLD) with a carbon nitride target and a negative bias voltage up to -120 V. The microstructure, chemical composition, bonding configuration and mechanical properties of the films were characterized by using scanning electron microscopy (SEM), X-ray diffraction (XRD), X-ray photoelectron spectroscopy (XPS), Raman spectroscopy, nanoindentation and ball-on-disc abrasion test. The results show that the negative bias voltage promotes the formation of sp<sup>3</sup> hybridization bonding and leads to a great improvement of nitrogen content (up to 38 at.%) in the films. With an increasing bias voltage from -40 V to -120 V, the nitrogen content and the fraction of sp<sup>3</sup> hybridization bonding

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decrease, leading to an increasing graphitization of the films. A direct dependence of the hardness on the content of sp<sup>3</sup> hybridization bonding is observed. The friction coefficient of the films ranges from 0.20 to 0.28. The film deposited at a bias voltage of -40 V presents the highest hardness value of 8.3 GPa.

*Keywords*: Carbon nitride; XPS; Raman; friction and wear; pulsed laser deposition

#### **1. Introduction**

Since Liu and Cohen [1] theoretically predicted that the crystalline phase  $\beta$ –C<sub>3</sub>N<sub>4</sub> could have bulk modulus and hardness comparable to or even higher than those of diamond, CN<sub>x</sub> films have received considerable interest. According to a large number of publications [2-9], CN<sub>x</sub> films are proved to be amorphous and the nitrogen content is far from the stoichiometric concentration (~57 at.%). Moreover, the mechanical properties of the films fluctuate in a large scale [10-13] and the thermal stability is poor due to its low decomposition temperature [14-16]. Nowadays, it is a tremendous challenge to fabricate a crystalline film that exhibits superhigh hardness in order to check the correctness of the theoretical prediction with of course tremendous application potential, though a few CN<sub>x</sub> films of high nitrogen concentration up to ~50 at. % (or N/C ratio ~1.0) have been synthesized by chemical vapor deposition (CVD) [17-18], electrodeposition [19], magnetron sputtering (MS) [20] and pulsed laser deposition (PLD) [21-23], *etc.* The optimal condition for the crystallization of carbon nitride is still to be found.

In recent years, our team has developed a series of pulsed laser deposited  $CN_x$  films by using a carbon nitride target instead of widely used graphite target. The results show that the nitrogen concentration of the films is greatly increased in comparison with those of conventional films deposited with graphite target, the growth rate of the films is more than twice as high as that of the conventional films and the size of particle lumps on the surface as well as the roughness of the films are reduced. However, the films exhibit a large value of  $x(sp^2C-N)/x(sp^3C-N)$  (*i.e.*, the mole content ratio of  $sp^2C-N$  bonding to  $sp^3C-N$  bonding) and lower mechanical properties compared to the conventional films. Due to the complexity of bonding configuration in  $CN_x$  films, it is quiet hard to conclude that a higher level of nitrogen content leads to lower mechanical properties. The importance of bonding configuration should be considered in the elaboration of high performance films.

It is well-known that the DC negative bias voltage technique is widely used in the magnetron sputtering deposition of films [24, 25]. The results show that the bias voltage dramatically affects the bonding configuration of carbon with/or nitrogen in the films [26, 27]. Consequently, by combining a negative bias voltage and the PLD technique, we can expect to alter efficiently the bonding configuration of the  $CN_x$  films deposited with carbon nitride target. In the present work, the  $CN_x$  films were fabricated in the deposition system. The composition, the chemical bonding states and the mechanical properties of the films were investigated by comparison with the films deposited using graphite target with the same process parameters.

#### 2. Experimental conditions

#### 2.1 Preparation of films and the target

 $CN_x$  films were deposited at room temperature by using a pulsed KrF excimer laser (Lambda Physik COMPex pro-201, wavelength of 248 nm, pulse duration of 25 ns, repetition rate of 10 Hz, and laser flux of ~6.7 J/cm<sup>2</sup>) with a carbon nitride target and a DC bias voltage value (*i.e.*,  $V_b$ ) of 0 V, -40 V, -80 V, -120 V, respectively. The negative bias voltage was applied to the sample holder insulated from the grounded chamber and the target. Polished Si<100> wafers were used as substrates and mounted onto the sample holder after being chemically cleaned. During the deposition, the pressure of N<sub>2</sub> (reacting gas, 99.999 % in purity) was set at 5 Pa and the target-to-substrate distance was 45 mm. The target and the

substrate were rotated to ensure the uniform erosion of the target and to improve the uniformity of the films. With a deposition duration of 20 minutes, the thickness of the films ranged from 1.1 to1.3  $\mu$ m. The CN<sub>x</sub> films for comparison purposes (*i.e.*, the reference films) were deposited by using graphite target (2.15 g cm<sup>-3</sup> in density) with the same process parameters as the films deposited with carbon nitride target. The film thickness ranged from 0.3 to 0.5  $\mu$ m.

The carbon nitride target was also fabricated by PLD technique with a silicon wafer substrate (50.8 mm in diameter and 420  $\mu$ m in thickness). Its deposition condition was the same as that of the reference films, except for the bias voltage of 0 V and the deposition duration of 520 hours. The thickness, density and the nitrogen concentration of the carbon nitride target are respectively 0.35 mm, 1.63 g cm<sup>-3</sup> and 24.5 at.%.

#### 2.2 Film characterization

The surface morphology and crystalline state of the films were observed by using scanning electron microscopy (SEM, Hitachi S-4700, with an accelerating voltage of 15 kV) and X-ray diffraction (XRD, Rigaku D/Max 115 2550PC, Cu K $\alpha$ , at an incidence angle of 3°, with a step of 0.02°). The XPS experiments were carried out with a Kratos AXIS Ultra DLD spectrometer, equipped with standard Al K $\alpha$  excitation source (*hv*=1 486.7 eV). The x-ray gun was operated at 300 W and photoelectron spectra were collected under constant pass energy of 20 eV for the analyzer. The energy calibration was referenced to the Cu 2p<sub>3/2</sub> line at 932.67 eV and the Ag 3d<sub>5/2</sub> line at 368.26 eV. After background subtraction of Shirley, the spectra were fitted with Lorentzian-Gaussian functions.

Raman scattering measurements (LabRAM HR UV) were performed by collecting the

backscattering radiation at excitation wavelength of 632.8 nm in the wave-number range of 800-2000 cm<sup>-1</sup>. After background subtraction by means of linear interpolation, the spectra were fitted with Lorentzian-Gaussian function. Nanoindentation tests were carried out on a Hysitron TI 900 triboindenter with Berkovich indenter and maximum load at 1 mN to evaluate the mechanical properties of the  $CN_x$  films. Each film was measured 20 times and the mean values of hardness and elastic modulus were calculated. The abrasion tests were carried out on a ball-on-disc tribometer (HT-600). The testing parameters were set as the following: Si<sub>3</sub>N<sub>4</sub> ball (5 mm in diameter), normal load at 0.49 N, sliding velocity at 0.176 m/s, test duration at 15 min, and relative humidity at 60~67%. The average values of the recorded instantaneous friction coefficient were used.

#### 3. Results and discussion

#### 3.1. Composition and chemical structure

The XRD results show that the films are amorphous. The typical surface morphology of the films is shown in Fig.1. It is similar for all  $CN_x$  films obtained with different bias voltages. This could be attributed to the rather weak bombardment effect of the PLD-ed species compared to Argon ions commonly used in ion etching technique. The kinetic energy of the former is about ( $V_b$ + 20~40) eV and the later is usually greater than 500 eV.

Fig.2 shows the detailed  $C_{1s}$  and  $N_{1s}$  XPS spectra of the films and the reference films as a function of bias voltage. According to some recent publications [28-32], the  $C_{1s}$  spectra (Fig. 2a) have been decomposed with Gaussian-Lorentzian distribution functions into five core level  $C_i$  (i=1,5):  $C_1$  284.5 ±0.1 eV,  $C_2$  285.3 ±0.2 eV,  $C_3$  286.3 ±0.1 eV,  $C_4$  287.4 ±0.2 eV, and  $C_5$  288.9 ±0.4 eV. The first two peaks are assigned as carbon coordinated carbon bonds

(respectively sp<sup>2</sup>C–C and sp<sup>3</sup>C–C). Due to the substitution of nitrogen for carbon in the carbon network, the C–N bonding configurations are presented at higher binding energies due to the higher electronegativity of nitrogen [33]. The contribution at 286.3 eV corresponds to the sp<sup>2</sup>C–N hybridization bonding, while the peak at 287.4 eV is attributed to the sp<sup>3</sup>C–N hybridization bonding. Finally, the peak C<sub>5</sub> is a characteristic of the C–O bonding configurations. In Fig.2b, the N<sub>1</sub> peak component (~398.6 ±0.1 eV) has been assigned to a sp<sup>3</sup>C–N hybridization bonding, meanwhile the N<sub>2</sub> peak (~400.0 ±0.1 eV) corresponds to a sp<sup>2</sup>C–N hybridization bonding, and the N<sub>3</sub> peak (~402.1 ±0.2 eV) corresponds to N–O bonding.

According to the deconvoluted results from the spectra above, the mole fraction of valence bonds can be determined, and then the ratio of  $x(sp^2)$  to  $x(sp^3)$  (calculated from C1s spectrum) and  $x(sp^2C-N)$  to  $x(sp^3C-N)$  (calculated from N1s spectrum) are illustrated as a function of bias voltage in Fig.3, where  $x(sp^2)$  is the mole fraction of  $sp^2$  bond,  $x(sp^3)$  the mole fraction of  $sp^3$  bond,  $x(sp^2C-N)$  the mole fraction of  $sp^2$  C–N bond, and  $x(sp^3C-N)$  the mole fraction of  $sp^3$  C–N bond. From Fig.3, both the ratio  $x(sp^2)/x(sp^3)$  and  $x(sp^2C-N)/x(sp^3C-N)$  of the films are strongly dependent on bias voltage, and the corresponding minima of 1.78 and 1.07 are obtained at -40V. It is suggested that the films deposited at -40V exhibit the highest mole fractions of both the sp<sup>3</sup> hybridization bonding and the  $sp^3C-N$  bonding. Both minima are obviously lower than those of the reference films (2.43 and 1.36, respectively). This indicates that the use of carbon nitride target can remarkably improve the content of  $sp^3$  hybridization bonding in the films. From Fig.3, we can also conclude that the bias voltage has an important influence on the bonding structure and the optimum bias voltage is around -40 V for promoting the formation of  $sp^3$  hybridization bonding in the films.

Fig.4 shows the effect of the bias voltage on the nitrogen content of the  $CN_x$  films. With the increase of bias voltage from 0 V to -120 V, the nitrogen content of the films peaks at -40V (~38 at.%) and is significantly higher than that of the reference films by 9~11 at.%. Accordingly, we can conclude that the use of carbon nitride target is beneficial to the formation of highly nitrogen-contained CN<sub>x</sub> films. Due to its relatively low density and heat of evaporation compared to graphite target, the carbon nitride target brings brighter and larger size plume during the ablation and yields a higher concentration of the species (e.g., C<sup>+</sup>, C<sub>2</sub><sup>+</sup>, CN,  $CN^+$ ,  $C_2N_2$ ,  $N^+$ ,  $N_2^+$ ) [34-36], which provoke more collisions among them. Under the condition without bias voltage, when carbon nitride target is sputtered physically, it is expected to have better composition transfer (therefore nitrogen content) from the target to the film. As a consequence of the chemical sputtering effect, the active carbon-containing species react with nitrogen, leading to the production of some CN radicals and C<sub>2</sub>N<sub>2</sub> which provide additional nitrogen atoms for the construction of CN<sub>x</sub> film. This is of course helpful for increasing nitrogen content in the film. This mechanism may explain why the nitrogen content in the films deposited with carbon nitride target is higher than that of its target. Now consider the film deposition under a bias voltage. On one hand, bias voltage provokes an increase of the kinetic energy of positively ionized species and consequently an increase of the chemical reactivity of these species. Therefore, the reaction between carbon-containing species and ambient nitrogen becomes easier and more nitrogen atoms can be incorporated into the film. On the other hand, bias voltage facilitates the refocusing on the film surface, of all positively ionized species (e.g.,  $N^+, N_2^+, CN^+, C_2N_2^+$ ) diverging from the deposition direction due to the collisions among the species. This refocusing will lead to an increase of the nitrogen content of the film. However, under the influence of the bias voltage, the positively ionized species in

the plasma are accelerated and driven towards the substrate and induce the actions of bombardment and sputtering on the film surface. At higher bias voltages, more intense bombardment of the species heats the substrate to a higher temperature, which releases the volatile nitrogen-containing molecules (*e.g.*, N<sub>2</sub>, C<sub>2</sub>N<sub>2</sub>) from the films [14-17]. Therefore, a further increase in bias voltage results in a reduction of nitrogen incorporation. Moreover, the size of the plume in the normal direction of target surface increases with an increase in bias voltage. Once the bias voltage exceeds a critical threshold (for instance, -550V in this case), the leading portion of the plume will be directly in contact with the films and leads to the destruction of the films by its high temperature.

Compared to the deposition of the reference films, more intense collision during the deposition will result in a decrease of the kinetic energy of the active species. And this will weaken the action of sputtering and bombardment, leading to a lower deposition temperature. It is well-known that sp<sup>3</sup> hybridization bonding is prone to be formed in the temperature range of 150-400 °C and it is also demonstrated that the fraction of sp<sup>3</sup> hybridization bonding decreases with bias voltage (Fig.3). Therefore we conclude that the higher fraction of sp<sup>3</sup> bonding of the films can be attributed to a relatively low deposition temperature and to an appropriate kinetic energy with which the deposited species arrive on the film surface.

Fig.5 shows the Raman spectra of the films. The measured spectrum of all films exhibits two asymmetric peaks with Gaussian functions similar to the Raman analysis of amorphous carbon in the range of 800-2000 cm<sup>-1</sup>. The peak centered at ~1350 cm<sup>-1</sup> is a disordered band (D band) originating from the  $A_{1g}$  breathing modes of sp<sup>2</sup> ring (hexagonal or graphitic) structures or the destruction of carbon networks by nitrogen substitution. The other peak centered at ~1530 cm<sup>-1</sup> is a graphitic band (G band) and attributed to the stretching of pairs of

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sp<sup>2</sup> atoms with vibrations ( $E_{2g}$  modes) [37,38]. After the deconvolution of Raman spectra of the CN<sub>x</sub> films, the detailed structural information of the films can be understood.

Fig.6 shows the dependence of the  $I_D/I_G$  (*i.e.*, the integral intensity ratio of D band to G band), the full width at half maximum of both D band and G band (i.e., FWHM<sub>D</sub> and FWHM<sub>G</sub>), and the position of both bands with bias voltage. As observed from Fig.6a, the slight shift of the G and D peak positions towards a higher wave band with the increase in bias voltage of  $CN_x$  films indicates an increase in the size of C sp<sup>2</sup> domains [39]. Meanwhile, the FWHM<sub>G</sub> of the films tends to decrease with higher bias voltage and this can be attributed to the increase of the cluster size [40]. The  $I_D/I_G$  ratio is a good structural indicator for  $CN_x$ films, since both  $I_D$  and  $I_G$  are sensitive to the size of the micro-domains. In fact,  $I_D$  and  $I_G$ decrease as the grain size increases [41]. It can be seen that the  $I_D/I_G$  ratio decreases at first and then increases with increasing bias voltage and the minimum  $I_D/I_G$  ratio of 1.85 is obtained at -40 V. According to A. Alkhawwam et al. [42] and A. C. Ferrari et al. [43], we can conclude that the increase in  $I_D/I_G$  ratio, the shift of the G and D peak positions towards higher frequencies, and the decrease in FWHM<sub>G</sub> with the increase of bias voltage can be attributed to the decrease in sp<sup>3</sup> bonding fraction and to the increase in size of graphitic cluster. At a bias voltage of -120 V, the high value of  $I_D/I_G$  and FWHM<sub>D</sub> of the film is attributed to the increasing bond angle disorder and indicate the increased degree of carbon network disorder [44, 45]. As for the reference films (Fig.6b), the higher values of the position of D and G bands and of the  $I_D/I_G$  ratio compared to those of the films deposited with carbon nitride target are mainly attributed to the lower sp<sup>3</sup> bonding fraction.

#### 3.2. Mechanical properties

Fig.7 shows the nanoindentation hardness and elastic modulus of CN<sub>x</sub> films deposited at different bias voltages. With the increase of bias voltage, the hardness increases initially and then decreases. Based on the fact that both ratio  $x(sp^2)/x(sp^3)$  and  $x(sp^2C-N)/x(sp^3C-N)$  follow exactly the opposite trend, we can conclude that the decrease of the ratio  $x(sp^2)/x(sp^3)$  and  $x(sp^{2}C-N)/x(sp^{3}C-N)$  makes a significant contribution to improving the hardness of CN<sub>x</sub> films [25-27]. The correspondence between bonding configuration and nanoindentation hardness can be explained by the formula  $H \sim (E_b \times a_c)/d^2$  (the hardness defined by the product of binding energy  $E_b$  and the covalency  $a_c$  divided by the square of bond length d) [46]. The short length and tetrahedrally bonded sp<sup>3</sup> hybridization bonding helps to build three-dimensional structure like diamond and makes CN<sub>x</sub> films more rigid [47]. However, the maximum film hardness of 8.35 GPa obtained at -40 V (5.1 GPa for the reference films) is much lower than the hardness reported in references [11-13, 48-50]. This indicates that these films exhibit a rather low resistance to penetration. Previous studies [10, 51] show that the  $CN_x$  film with a nitrogen concentration between 35-50 at.%, a low density and a polymer-like structure exhibits a rather low hardness and elastic modulus than most films. It is possible that the films deposited at -80V and -120V are similar to these films, because more intense bombardment of species on the film surface leads to a decrease in density and to the structure alteration from compact carbon network to the polymer-like structure.

Fig.8 shows the mean value of friction coefficient of the  $CN_x$  films against Si<sub>3</sub>N<sub>4</sub> ball in humid air. At the function of bias voltage, the friction coefficient of the films addresses the highest value of 0.28 at -40 V and falls slowly later, but is greater than that of the reference films by 0.02~0.06 typically. We believe that, under the same test conditions and tribological mechanism, the sp<sup>2</sup> hybridization component is easier to be sheared and contributes to low friction coefficient during wear tests, but the sp<sup>3</sup> hybridization component presents an opposite action. When the content of sp<sup>3</sup> hybridization component decreases in the films, the resistance force in sliding tests decreases and the friction coefficient of the films becomes smaller. Therefore, an increase of the ratio  $x(sp^2)/x(sp^3)$  of the films leads to a lower friction coefficient. Therefore, the reference films exhibits a low friction coefficient due to the fact that they have a relatively high level of the  $x(sp^2)/x(sp^3)$  ratio, compared to the films deposited with carbon nitride target.

#### 4. Conclusions

The microstructure and mechanical properties of the  $CN_x$  films prepared by PLD with negative bias voltage and carbon nitride target were studied. The nitrogen content and the fraction of sp<sup>3</sup> hybridization bonding in the films are remarkably improved by using the hybrid deposition system. The nitrogen content as well as the  $x(sp^2)/x(sp^3)$  and  $x(sp^2C-$ N)/ $x(sp^3C-$ N) ratio of the films are obviously dependent on the bias voltage value. With the increase of bias voltage from -40 V to -120V, an increased graphitization of the films is observed, accompanied by a decrease of the hardness, the elastic modulus and the friction coefficient of the films. The maximum hardness of 8.35 GPa is obtained with a bias voltage of -40 V.

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## **Figure captions**

- Fig. 1 The SEM image of  $CN_x$  film deposited at bias voltage of -40 V
- Fig. 2 The  $C_{1s}$  and  $N_{1s}$  XPS spectra of  $CN_x$  films deposited by various bias voltages
- **Fig.3** Dependence of the ratio of  $x(sp^2)/x(sp^3)$  in C<sub>1s</sub> XPS spectrum and  $x(sp^2C-N)/x(sp^3C-N)$ 
  - in N<sub>1s</sub> XPS spectrum with negative bias voltage.  $x(sp^2)$ -Mole fraction of  $sp^2$  bond,  $x(sp^3)$ -Mole fraction of  $sp^3$  bond,  $x(sp^2C-N)$ -Mole fraction of  $sp^2$  C–N bond,  $x(sp^3C-N)$ -Mole fraction of  $sp^3$  C–N bond.
- Fig. 4 Nitrogen content in the films as a function of bias voltage
- Fig. 5 Deconvolution of Raman spectra of the  $CN_x$  films deposited at different bias voltages
- **Fig.6** Variations of the  $I_d/I_g$ , FWHM and position of D band and G band of the CN<sub>x</sub> films with bias voltage
- Fig.7 Effects of bias voltage on the hardness and elastic modulus of CN<sub>x</sub> films
- Fig.8 Effects of bias voltage on the friction coefficient of CN<sub>x</sub> films

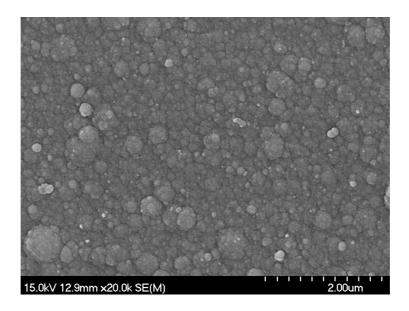
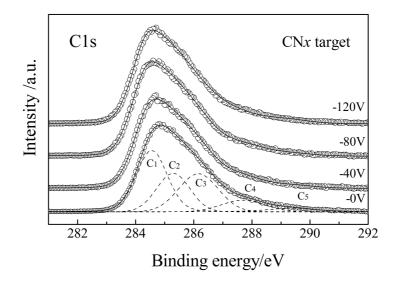
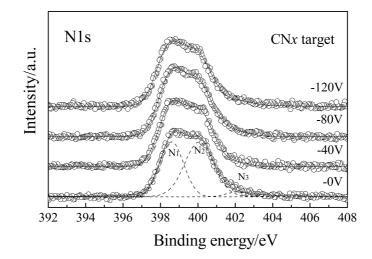


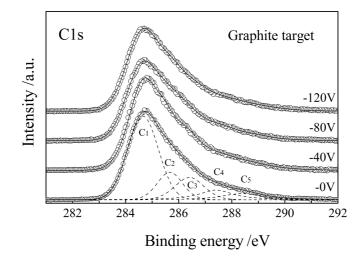
Fig. 1



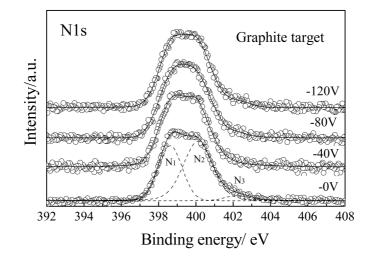
(a) C1s, Carbon nitride target



(b) N1s, Carbon nitride target



(c) C1s, Graphite target



(d) N1s, Graphite target

Fig. 2

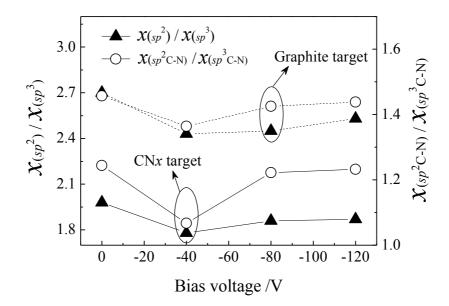


Fig. 3

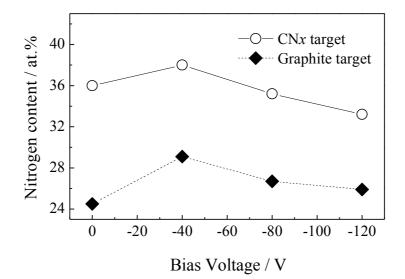
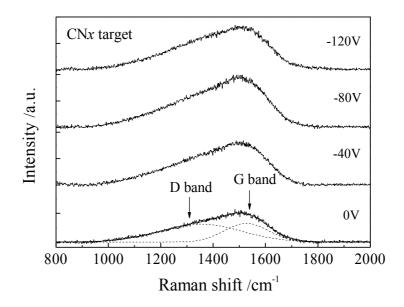
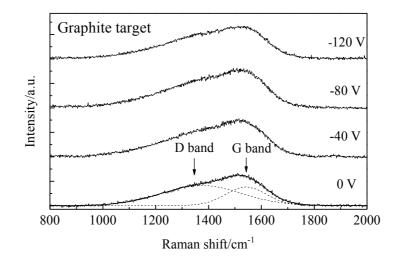


Fig. 4

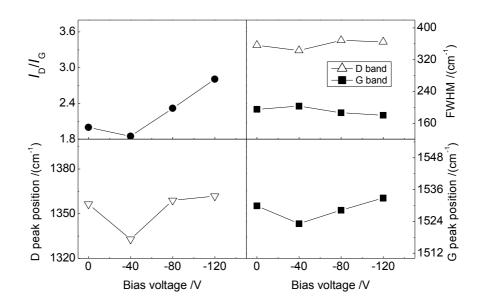


(a) Carbon nitride target

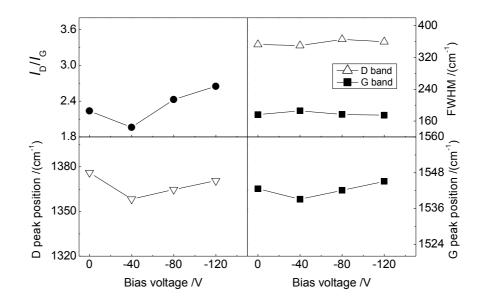


(b) Graphite target

Fig. 5



(a) Carbon nitride target



(b) Graphite target

Fig. 6

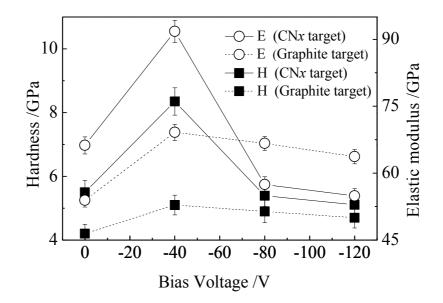


Fig. 7

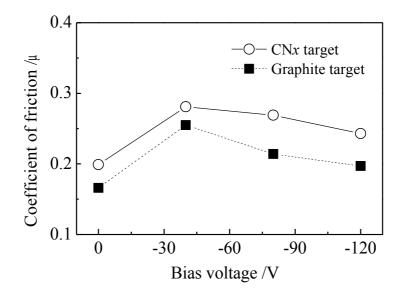


Fig. 8